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TRANSONIC AERODYNAMIC CHARACTERISTICS OF A WING/BODY COMBINATION INCORPORATING JET FLAPS

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CHARACTERISTICS OF A WING/BODY COMBINATION

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## TRANSONIC AERODYNAMIC CHARACTERISTICS OF A WING/BODY COMBINATION INCORPORATING JET FLAPS

John L. Holmberg

Ames Research Center

#### SUMMARY

A 0.25-scale semispan wing/body model with two types of jet flaps proposed by Rockwell International was tested in the Ames II- by II-Foot Transonic Wind Tunnel. The objective of that testing was to measure the static aerodynamic forces and moments and wing pressure distributions on six configurations differentiated by wing camber, jet flap type, and jet flap angle. Maximum thrust coefficients were limited to 0.12. Angle of attack was varied from -4° to 15° for Mach numbers between 0.6 and 0.95 at a constant unit Reynolds number of 18.0 million/m (5.5 million/ft).

Due to the limited scope of this test and in the absence of any rigorous analysis, no final conclusions should be drawn concerning the relative effectiveness of the two flap systems. More refined designs and considerably more testing will be required even to establish the practicability of the total-exhausting jet flap concept.

#### INTRODUCTION

One of the basic goals for the next generation of fighter aircraft is increased maneuverability in the transonic flight regime. One approach to achieving this goal involves ducting the total engine exhaust out through the trailing edges of the wings, thereby providing both thrust and a jet flap effect to increase lift without incurring a large induced drag penalty. Rockwell International has proposed two methods for controlling the effective angle of total-exhausting jet flaps. The first method, the Trapped Flow (TF) flap, turns the exhaust flow by deflecting the whole internal duct/external airfoil structure along the 62.5 percent chordline. The second method, the Augmented Deflected Exhaust Nozzle (ADEN) flap, keeps the entire internal duct in a fixed position; the upper surface of the airfoil section, being 5.5 percent longer in chord than the lower surface and hinged along the top edge of the duct exit, acts as a deflector plate to turn the emerging jet. Each of these total-exhausting jet flap systems is intended to be used with a variable leading-edge-camber airfoil. Both flap concepts were tested in the Ames 11- by 11-Foot Transonic Wind Tunnel. Presented herein are results from that investigation with minimal analysis.

# SYMBOLS

Standard body and stability axis systems and sign conventions are shown in figure 1. All force and moment coefficients include thrust effects.

Symbol .	Definition
AE	jet exit area
A(i)	base areas (i = 1 through 8)
ALPHA	wing angle of attack, deg
В	wing span
BETA	angle of yaw (always 0 deg)
С	local wing chord
č	mean aerodynamic chord
CD	<pre>drag coefficient = drag corrected for base pressure/Q (S/2)</pre>
CL.	<pre>lift coefficient = lift corrected for base pressure/Q (S/2)</pre>
CLM	pitching moment coefficient = pitching moment about model station 1.4487 m (57.036 in) corrected for base pressure/Qc (S/2)
CONF	configuration number
CP	<pre>pressure coefficient = (local pressure - PINF)/Q</pre>
CTG	thrust coefficient = $(FGST + (PO-PINF)AE)/Q (S/2)$
DELFI	inboard jet flap angle, deg
DELFM	leading-edge flap angle, deg
DELFO	outboard conventional flap angle, deg
DELJ	effective jet angle, deg

Symbol	<u>Definition</u>
FGSTLB	static thrust, 1b
FGSTNT.	static thrust, N
MACH	free-stream Mach number
PINF	free-stream static pressure
PO	ambient pressure during static thrust calibration
Q	free-stream dynamic pressure
RN/L	free-stream unit Reynolds number, millions/ft
RN/M	free-stream unit Reynolds number, millions/m
S	wing reference area
X	distance along local chord from leading edge
Υ	distance along span from fuselage centerline

#### TEST FACILITY

The Ames 11- by 11-Foot Wind Tunnel is a closed-return, continuous-flow, variable-density tunnel with a flexible-wall nozzle. All four walls enclosing the test section are ventilated with porous slots of 5.6 percent open area ratio to permit operation over a Mach number range continuously variable from 0.4 to 1.4. During this test, however, the slots in the floor were covered with tape to form an image plane for the semispan model.

#### MODEL DESCRIPTION

The 0.25-scale left-hand wing and left fuselage half were mounted above a nonmetric spacer to raise the centerline of the model above the displacement thickness of the boundary layer on the tunnel floor (fig. 2). Both the TF flap and the ADEN flap extended over the inboard 50 percent of the exposed span(fig. 3). A conventional flap on the cranked portion of the wing remained at zero deflection for all but one configuration. The basic airfoil section had a maximum thickness to chord ratio of 8.5 percent at the 20 percent chord position and a maximum camber of 2 percent at the 50 percent chord position; the inboard portion of the trailing edge was opened just enough to accommodate the jet flap ducts

(fig. 4). Full-span, segmented leading-edge flaps were used to effect variable camber, and angle blocks were inserted between the wing and the TF or ADEN flaps to represent deflections about fixed hinge lines (fig. 5). The specific combinations of leading-edge deflection, jet flap type, and jet flap angle associated with the six configurations tested are described in table 1. The locations of the 164 static pressure orifices positioned along chordlines at 4 span stations are indicated in table 2.

#### TESTING AND DATA REDUCTION PROCEDURES

The complete wing/body combination (figs. 6 and 7) was mounted on a five-component strain gage balance which was submerged beneath the floor of the test section. High pressure air simulating engine exhaust was supplied to the model through a piping system which bridged the balance (fig. 8). A complete balance calibration was performed in the tunnel at the beginning of the test with all of the high pressure fittings connected to account fully for the influence of the piping bridge on primary sensitivities and interactions between components.

Before each configuration was tested, a static thrust calibration was performed with the tunnel off to evaluate the magnitude and direction of the jet flap thrust vector at blowing rates of up to 5 kg/s (II lb-mass/s). Flow rates were measured by a sonic nozzle flowmeter upstream of the balance assembly. During these calibration runs, flow inhibitor fences were positioned perpendicular to the wing just ahead of the jet flap to minimize induced flow and associated aerodynamic loads.

Static force and moment data were recorded for each configuration at angles of attack from -4° to 15° with Mach numbers in the range 0.6 to 0.95 at a constant unit Reynolds number of 18.0 million/m (5.5 million/ft). Wing pressure distributions were recorded at angles of attack of 0°, 4°, 8°, 12°, and 15° for specific configuration number/Mach number combinations as shown in table 3. Natural boundary layer transition from laminar to turbulent conditions was permitted throughout the test.

All force and moment coefficients presented in this report include the effects of jet flap thrust. Those coefficients are corrected for an effective base pressure which was determined in the following manner:

Effective base pressure coefficient =  $(2/S) \sum CP(i) A(i)$ 

Jet Off: i = 1 through 8

Jet On: i = 7, 8

where i = 1 through 6 denote the six cavities within the jet flap duct exit and i = 7, 8 denote base areas along the trailing edge of the wing

(table 4). Pitching moment coefficients are always referenced to model station 1.4487 m (57.036 in).

#### RESULTS AND DISCUSSION

A complete index of all data figures is included in table 5. However, several points concerning information presented in those figures warrant special comment.

Rockwell International's method of supplying high pressure air to the model introduced two potential sources of inaccuracy into the measurement of forces and moments. Those sources were mechanical hysteresis in the joints at each end of the piping bridging the balance and thermal gradients in the balance due to the expansion of high pressure air into a plenum which was mounted directly to the top of that balance. Data recorded under identical test conditions before and after long series of blowing and nonblowing runs did show evidence of shifts in the zero-load reference output voltage levels of the strain gage bridges (fig. 9). Such zero shifts could have been attributable to either source. A special series of data points was generated to evaluate the maximum anticipated imprecisions resulting from zero shifts. With the wind tunnel not running, balance readings were recorded periodically during 10 min jet-on (maximum blowing rate)/jet-off cycles. Measured forces and moments were reduced to coefficient form based on an artifical Q of  $47800 \text{ N/m}^2$  [1000 lb/ft²; see fig. 10(a)]. A thermocouple mounted on the balance near the upper set of strain gages monitered changes in temperature during those same cycles [fig. 10(b)]. The results of that special series indicated that representative precisions of data presented in this report are CL + 0.012, CD ± 0.0030, and CLM + 0.002.

An effective jet angle DELJ was defined as a function of jet mass flow rate during the static thrust calibration of each configuration (fig. 11). This angle was resolved from balance data as follows:

DELJ = Arctan (normal force/axial force)

Maximum axial forces recorded during the calibrations were approximately 70 percent of balance capacity for that component. However, the corresponding normal forces were less than 3 percent of capacity. As a result, the accuracy of the determination of DELJ was quite poor. The simple geometric inboard jet flap angle DELFI was a more meaningful indicator of the probable jet angle.

Several blowing and nonblowing runs were conducted at a unit Reynolds number of 13.1 million/m (4.0 million/ft). The changes noted between data recorded at the two Reynolds numbers were generally predictable.

Decreasing the Reynolds number increased drag, reduced the lift curve slope, and moved the center of pressure forward (fig. 12).

The basic wing/body/TF flap configuration (2) was stable at all conditions tested; maximum blowing rates increased its lift curve slope by roughly 10 percent (fig. 13). Drooping the leading edge of the wing 8° (configuration 3) delayed the onset of separation at higher angles of attack, moved the center of pressure aft, and increased the lift curve slope by 8 to 10 percent. Deflecting the TF flap and conventional outboard flap to 3.5° (configuration 4) increased CL uniformly by 0.07 over the ALPHA range studied and increased both stability and minimum drag.

The basic ADEN flap configuration (5) had a slightly lower minimum drag than the corresponding TF flap configuration (3); however its CL at zero angle of attack and lift curve slope were lower, and it was less stable. The ADEN flap responded to blowing with a positive shift in CL but with little change in lift curve slope. The TF flap responded to blowing in just the opposite manner. Increasing ADEN flap deflections (configurations 6 and 7) without blowing shifted CL positively and moved the center of pressure aft. Maximum blowing rates increased lift increments substantially beyond those attributable to nonblowing ADEN flap deflections and/or direct thrust effects; this result was especially noticeable at lower Mach numbers (fig. 14).

None of the configurations tested demonstrated any particular sensitivity of lateral center of pressure to blowing rate (figures demonstrating this fact were deemed too trivial for presentation). However, the other integrated aerodynamic characteristics previously discussed are reflected in the individual chord-wise pressure distributions recorded over both surfaces of the wing (fig. 15).

#### CONCLUDING REMARKS

Due to the limited scope of this test and in the absence of any rigorous analysis, no final conclusions should be drawn concerning the relative effectiveness of the TF and ADEN flap systems. More refined designs and considerably more testing will be required even to establish the practicability of the total-exhausting jet flap concept. However, some valuable lessons in blowing, semispan model testing techniques were learned. The most significant of those lessons was that the balance must be effectively insulated from the model whenever high pressure air is expanded to ambient conditions producing severe localized cooling. Based on the results of this and related tests, Ames has developed specialized servo-controlled heaters which maintain preset temperature differentials between the model, balance, and pressure lines. With these heaters thermally isolating the model from the balance and proper thermal compensation within the individual balance bridges, simulations of jets at higher pressures with higher

mass flow rates will no longer compromise the accuracy of aerodynamic force measurements.

Ames Research Center National Aeronautics and Space Administration Moffett Field, California 94035

August 21, 1975

TABLE 1. - CONFIGURATION DEFINITIONS

Configuration number	Flap type	DELFI, deg	DELFO, deg	DELFM deg
2	TF	0	0	0
3	TF	0	0	8
4	TF	3.5	3.5	8
5	ADEN	0	0	8
6	ADEN	15	0	8
7	ADEN	30	0	8

TABLE 2. - WING STATIC PRESSURE ORIFICE LOCATIONS (DELFM =  $8^{\circ}$ )
Locations are given as decimal fractions of local chord length (X/C).

		Upper Surfac	ce	·		Lower Surfa	ace	
2Y/B =	.25	.45	.65	.80	.25	.45	.65	.80
	0	0	0	0				
	.023	.023	.022	.022	.023	.023	.022	b .022
	.046	.046	.044	.044	.046	.046	.044	.044
	.069	.068	.067	.066	.069	.068	.067	.066
	.092	.091	.089	.088	.092	.091	.089	.088
	.139	.137	.133	.132	.185	.182	.178	.176
	.185	.182	.178	.176	a .278	a .274	a .268	a .269
	.231	.228	,222	.220	.353	.362	.377	.384
	a .273	a .265	a .268	a .255	.445	.454	.466	b .472
	a .303	a .320	b .300	a .300	.538	.545	.555	.560
	.353	.362	a .330	a .340	.630	.636	.644	.648
	.399	.408	.377	.384	.723	.772	.733	.736
	.445	.454	.422	.428	.815	.818	.822	.824
	.491	.499	.466	.472	.861	.863	.867	.868
	.538	.545	.511	.516	.908	.909	. <del>9</del> 11	.912
	.584	.590	.555	.560	.935	.935	.956	.956
	.630	.636	.600	.604				
	ь.676	b .681	.644	.648	a An oi	rifice not o	on configura	ation 2.
	.723	.727	.689	.692				
	.769	b .772	b .733	.736	b An oi	rifice plugg	ged througho	out the test
	.815	.818	.778	.780			_	
	.861	.863	.822	.824	c An oi	rifice on th	he ADEN flap	only.
	.908	.909	.867	.868			•	<del>-</del>
	c .939	c .939	.911	.912				
	. 954	.954	.956	.956				
	c .984	c .984						
	c .988	c .988						

ď.

TABLE 3. - TEST CONDITIONS SUMMARY

CONF	ALPHA	CTG	RN/L				MA	CH NUMBER			
	· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	0	0.6	0.7	0.8	0.875	0.9	0.925	0.95
2 2 2	0 A A	V 0 .04 .08	0 5.5 5.5	F	F	F,P	F	F	F,P F	F	F,P
2 2 3 3	A A A	.12 0 .12	5.5 5.5 5.5 5.5 5.5	_		F,P F,P F	F F F		F,P F,P F		F.P F.P F.
4 4 4	0 A A	ν	0 5.5 5.5 5.5 5.5	F	F	F,P	F	F	F,P		F,P
4 4 4 4	A A A	.04 .08 .12 0 .12	4.0 4.0	• • • •		F,P F F	F		F,P F F		F,P
5 5 5 5	0 A A A	V 0 .04 .08 .12	0 5.5 5.5 5.5 5.5	F	· ·* · · · ·	F F F			F,P F,P* F,P		F F F
6 6 6	0 A A	V 0 .04 .08 .12	5.5 5.5 5.5 5.5	F		F F F	· ;		F,P F,P* F,P*		F
6 7 7 7	A O A A	.12 V 0 .04 .08 .12	5.5 0 5.5 5.5 5.5 5.5	F		F F F	i a	+ <u>;</u>	F,P F,P* F,P* F,P		F
7	A A	.08 .12	5.5 5.5			F F			F,P* F,P	·	

aSchedules:

A = -4, -3, -2, -1, 0, 1, 2, 3, 4, 5, 6, 7, 8, 10, 12, 14, 15, 0 deg. V = Static thrust calibration, 0 < CTG < 0.12.

F = Force data.

P = Pressure distributions at 0,4,8,12,15 deg. P\*= Pressure distributions at 4 deg. only.

TABLE 4. - REFERENCE DIMENSIONS

Base area	Configur	ations 2-4	<u>Configura</u>	tions 5-7
A(1)	0.000953 m <sup>2</sup>	(0.01026 ft <sup>2</sup> )	0.001131 m <sup>2</sup>	(0.01218 ft <sup>2</sup> )
A(2)	0.000848	(0.00912)	0.000864	(0.00930)
A(3)	0.000772	(0.00831)	0.000795	(0.00856)
A(4)	0.000709	(0.00763)	0.000719	(0.00774)
A(5)	0.000620	(0.00668)	0.000632	(0.00680)
A(6)	0.000578	(0.00621)	0.000696	(0.00749)
A(7)	0.000185	(0.00200)	0	(0)
A(8)	0.000084	(0.00090)	0	(0)
AE	0.003942	(0.04243)	0.004066	(0.04376)

Wing span = 1.3737 m (4.5069 ft)

Mean aerodynamic chord = 0.5920 m (1.9421 ft)

Wing reference area =  $0.7548 \text{ m}^2 (8.125 \text{ ft}^2)$ 

## TABLE 5. - INDEX OF DATA FIGURES

Figure	Caption	Page
9	Repeatability evaluation.	21
10(a)	Effects of jet-on jet-off cycling on wind-off balance zeros.	25
10(b)	Balance temperature at upper gages during jet cycling.	26
11	Static thrust calibration.	27
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14	Flap effects.	74
15	Pressure distributions.	86

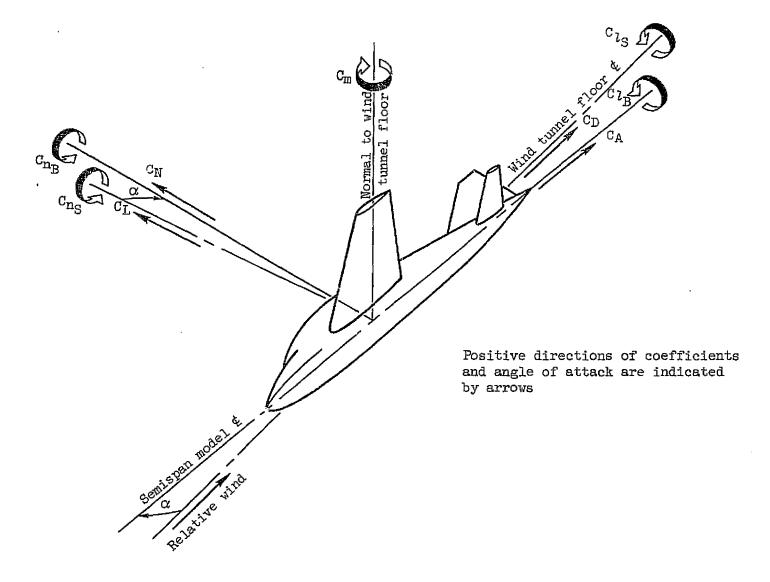


Figure 1. - Definition of axis systems for a semispan model.

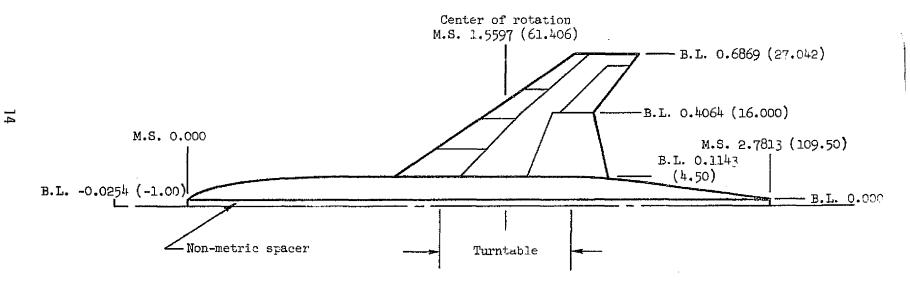


Figure 2. - Model installation schematic.

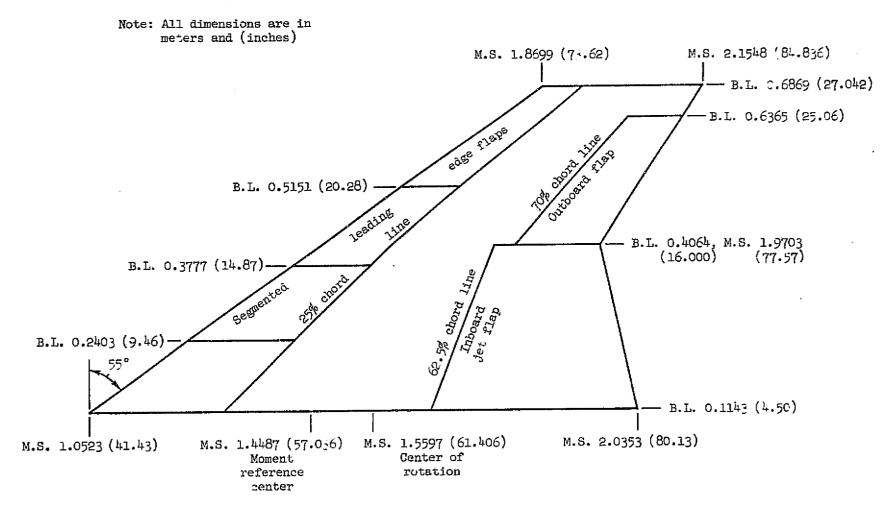


Figure 3. - Wing planform details.

## Wing reference plane

Outboard section

No leading edge or flap deflections shown for either section

Wing reference plane (WRP)

Inboard section

Figure 4. - Representative airfoil sections.

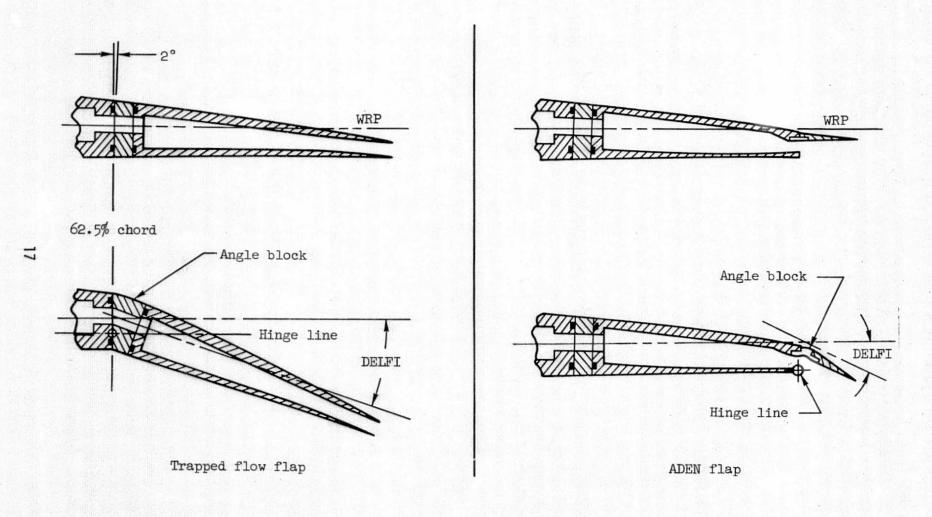


Figure 5. - Comparison of Trapped Flow and ADEN flaps.

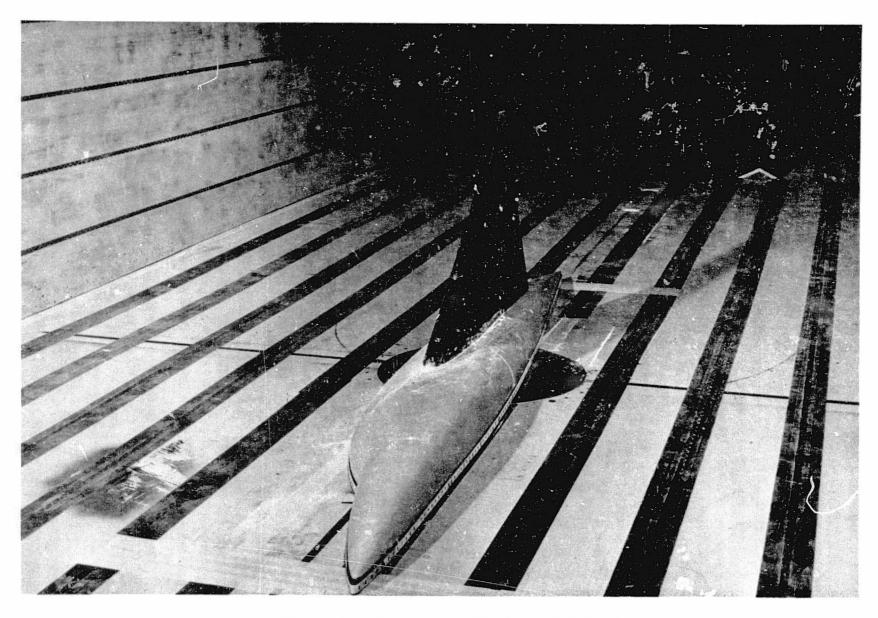


Figure 6. - Tunnel installation - 3/4 front view.

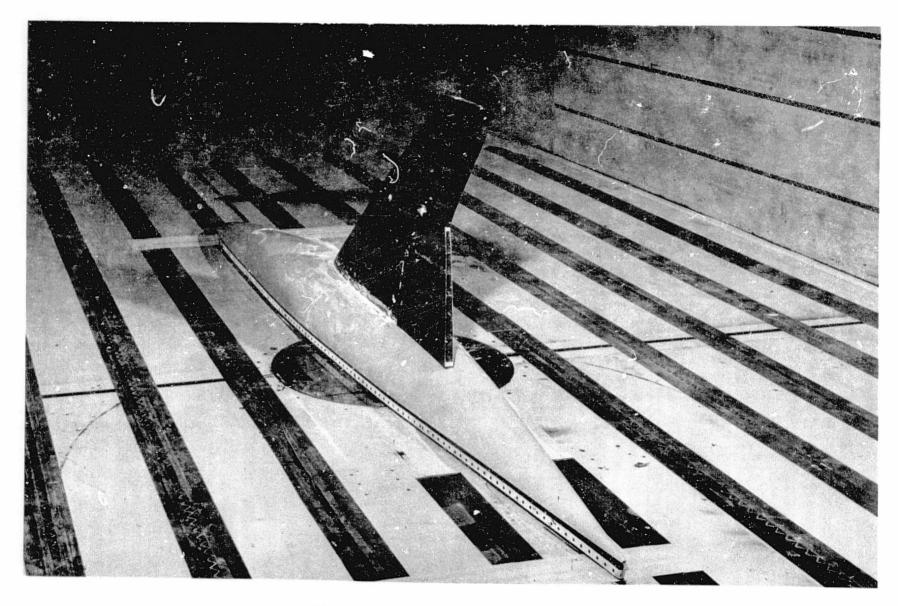


Figure 7. - Tunnel installation - 3/4 aft view.

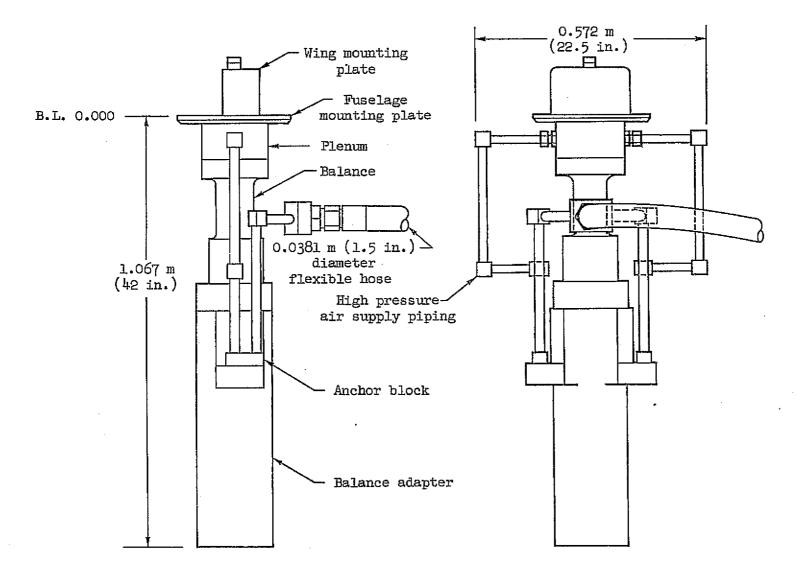


Figure 8. - High pressure air supply system schematic.

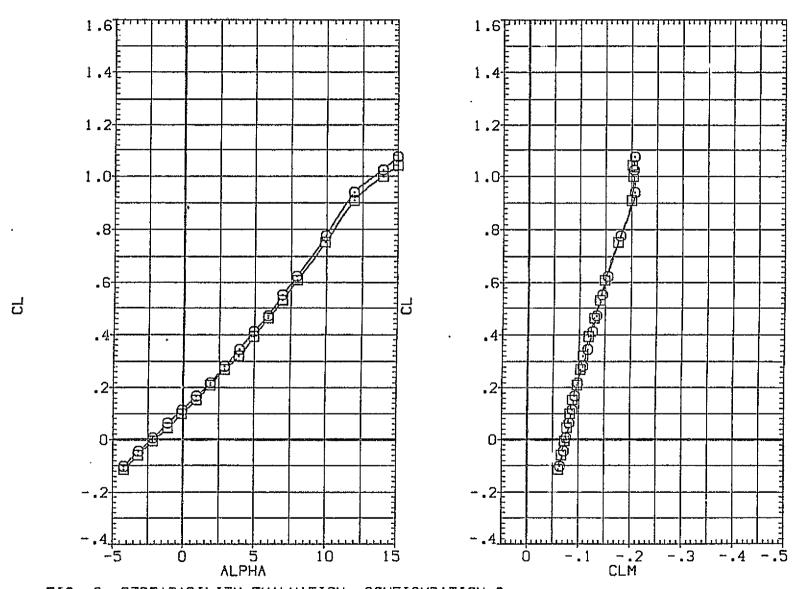


FIG. 9 REPEATABILITY EVALUATION- CONFIGURATION 2

(A)MACH = .70

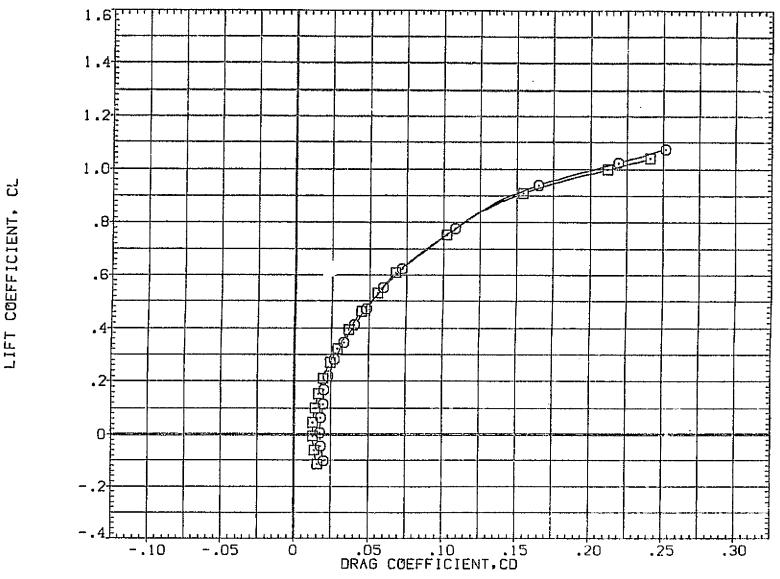


FIG. 9 REPEATABILITY EVALUATION- CONFIGURATION 2

(A)MACH = .70

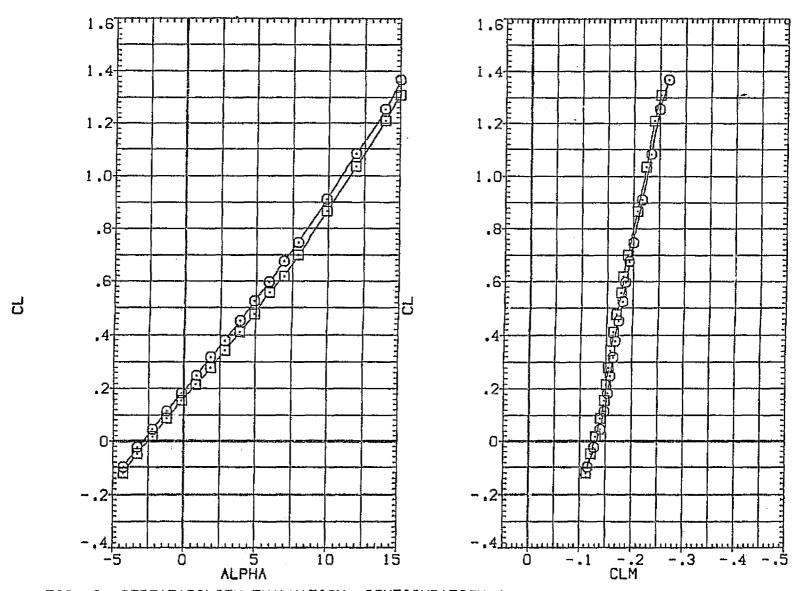


FIG. 9 REPEATABILITY EVALUATION— CONFIGURATION 4

(A)MACH = .70

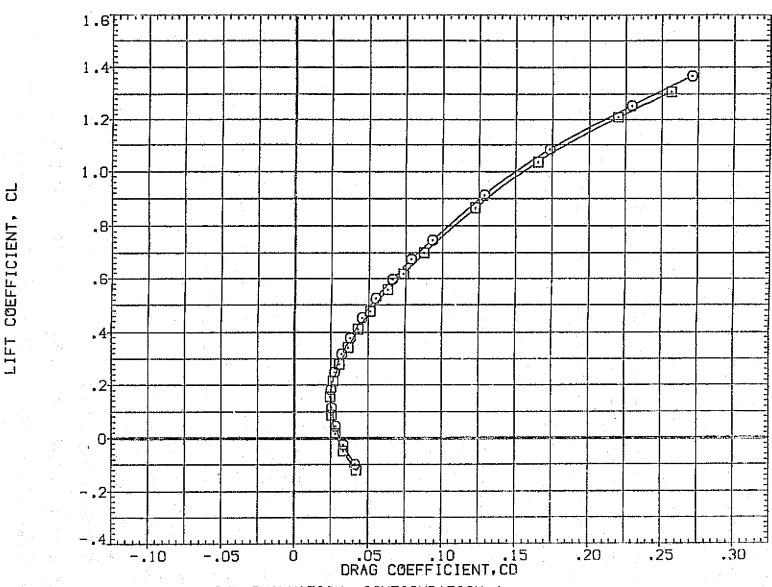


FIG. 9 REPEATABILITY EVALUATION- CONFIGURATION 4

(A)MACH = .70

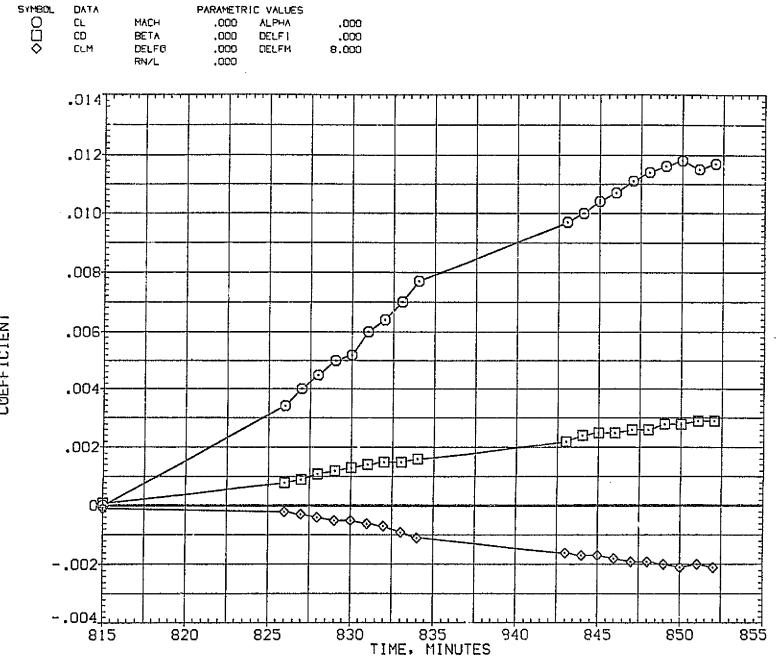


FIG. 10A EFFECTS OF JET-ON/JET-OFF CYCLING ON WIND OFF BALANCE ZEROS

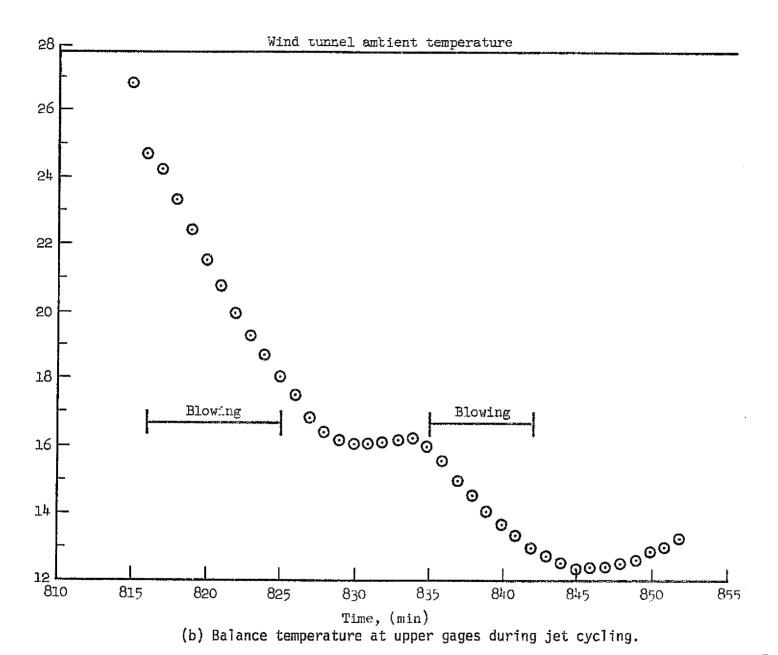


Figure 10. - Concluded.

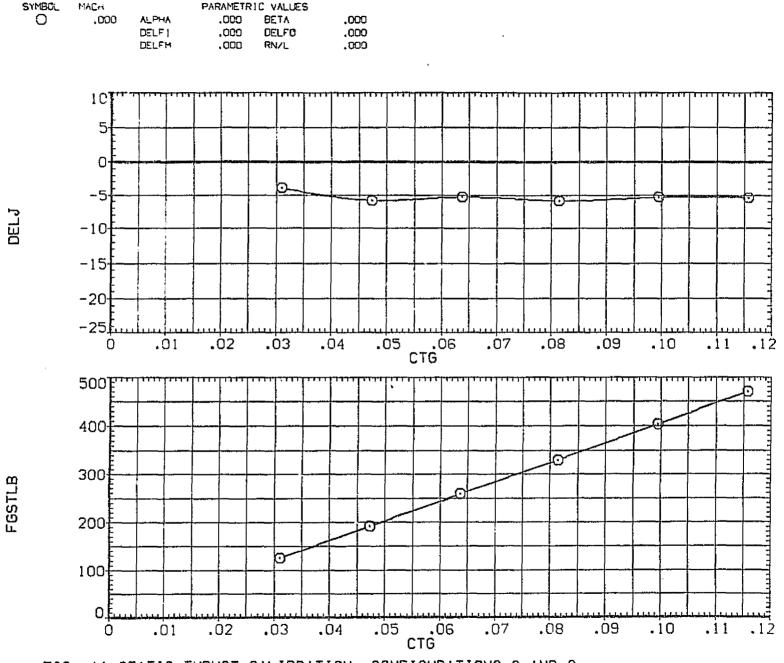


FIG. 11 STATIC THRUST CALIBRATION- CONFIGURATIONS 2 AND 3

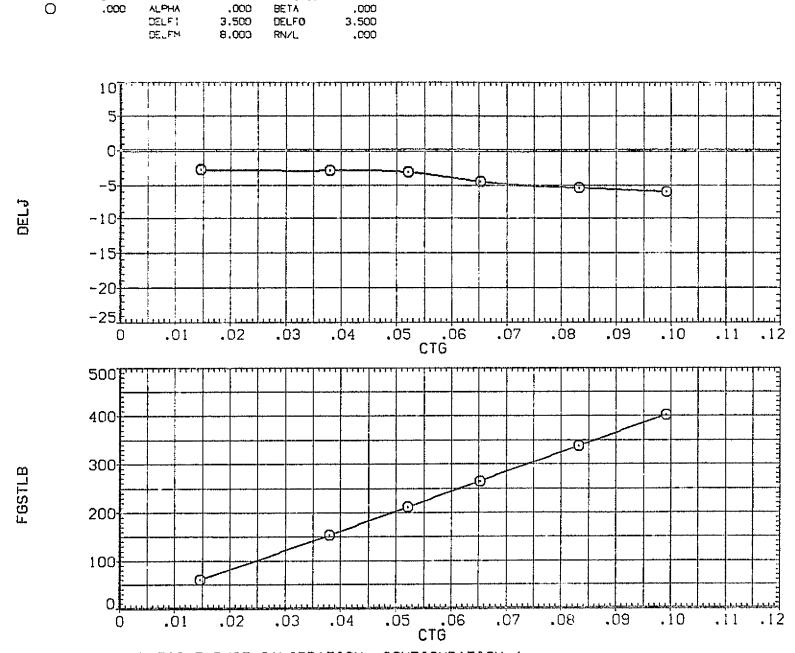


FIG. 11 STATIC THRUST CALIBRATION- CONFIGURATION 4

PARAMETRIC VALUES

.000

SYMBOL

3

MACH

.000

ALPHA

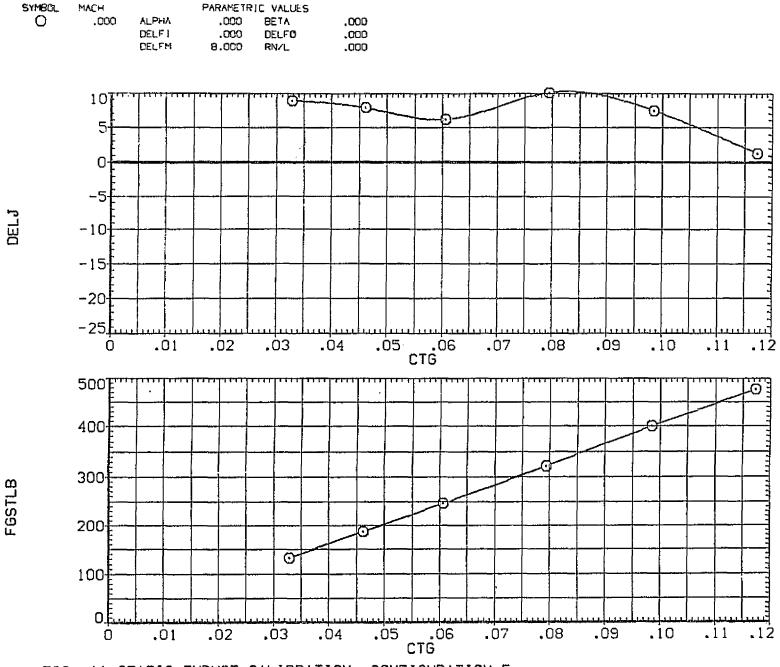


FIG. 11 STATIC THRUST CALIBRATION- CONFIGURATION 5

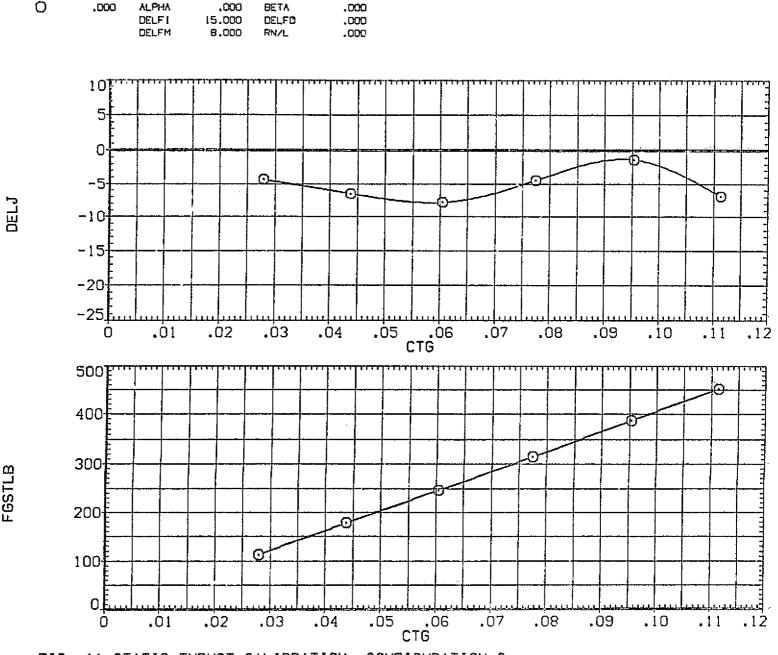


FIG. 11 STATIC THRUST CALIBRATION- CONFIGURATION 6

PARAMETRIC VALUES

BETA

SYMBOL

MACH

ALPHA

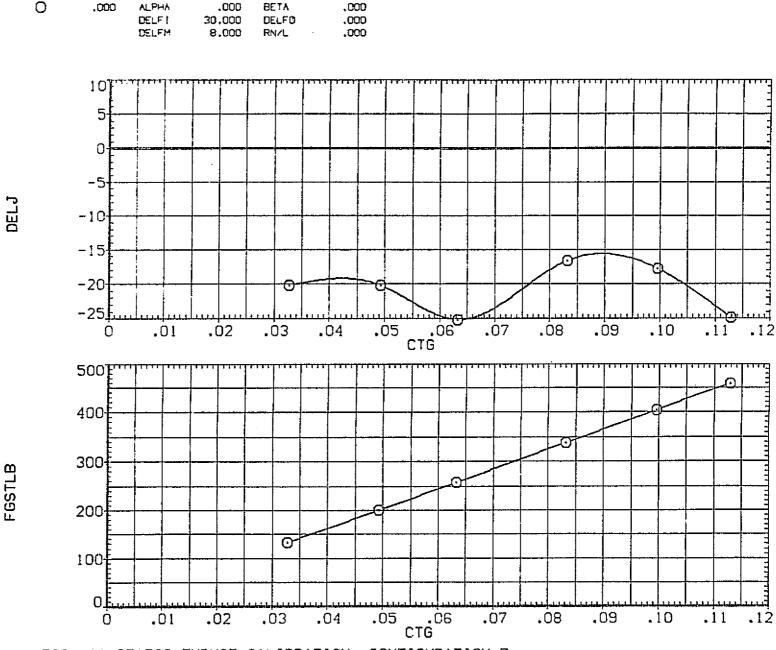


FIG. 11 STATIC THRUST CALIBRATION- CONFIGURATION 7

PARAMETRIC VALUES

SYMBOL

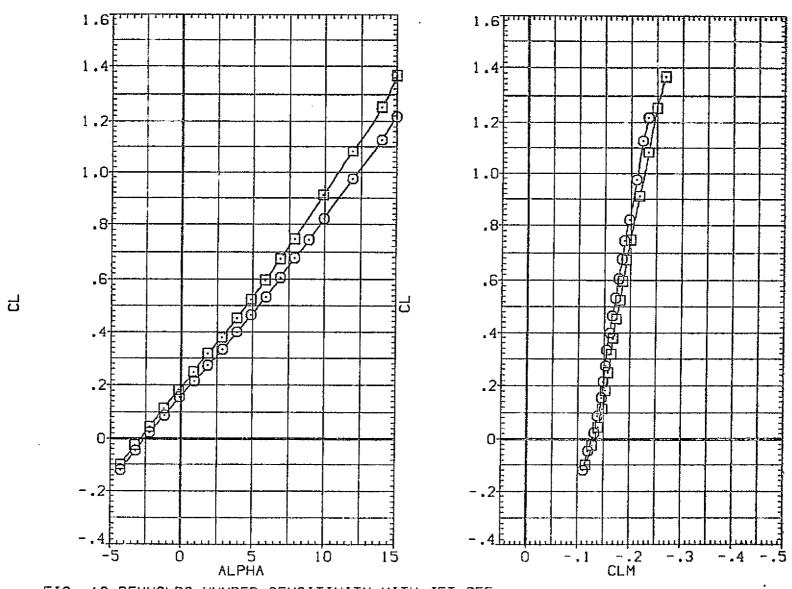


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET OFF

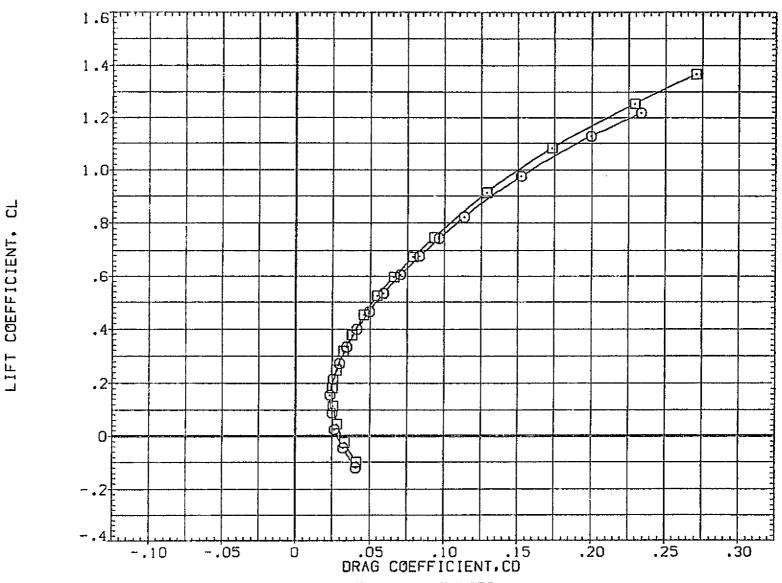


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET OFF

(A)MACH = .70

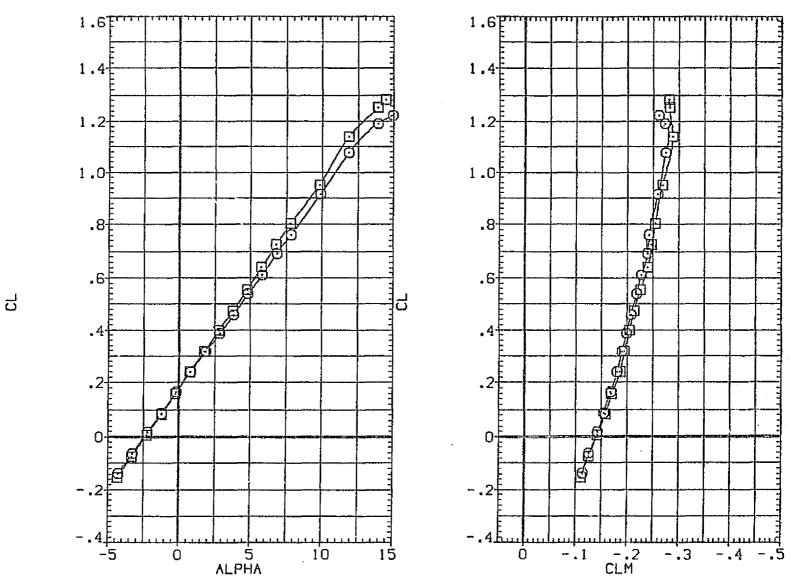


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET OFF
(B)MACH = .90

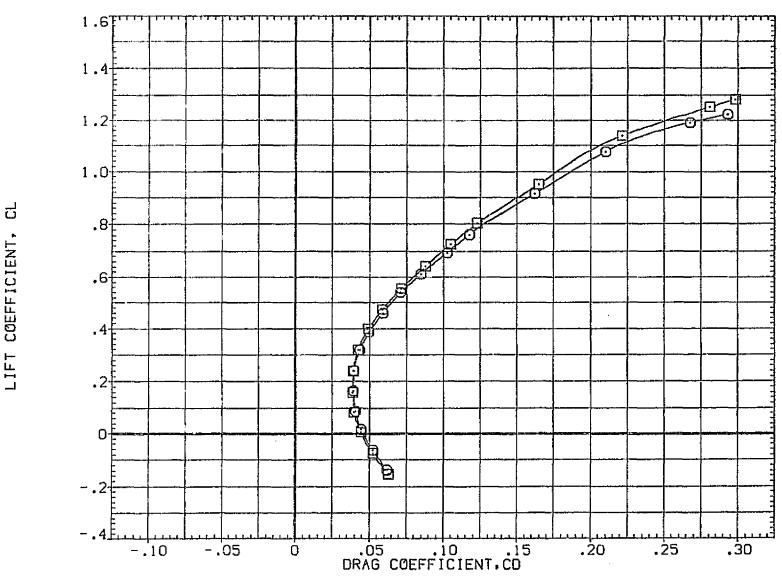


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET OFF (B)MACH = .90

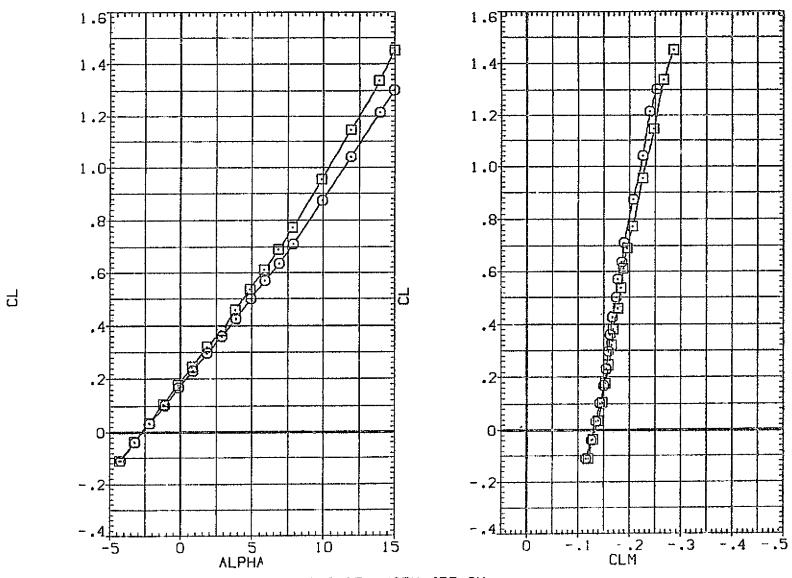


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET ON

(A)MACH = .70

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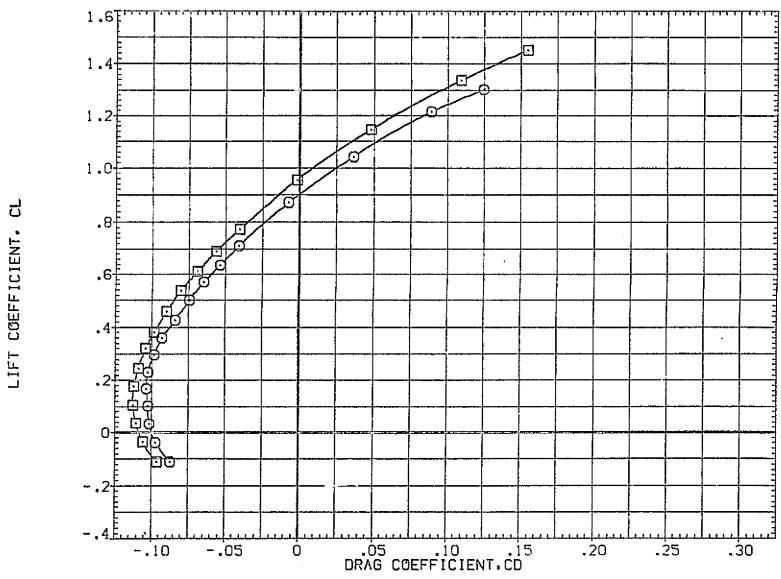


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET ON

yaran iliyenin matalan iliya matalan alika balan iliya matalan <del>alimba taha asala alika balan balan balan balan</del>

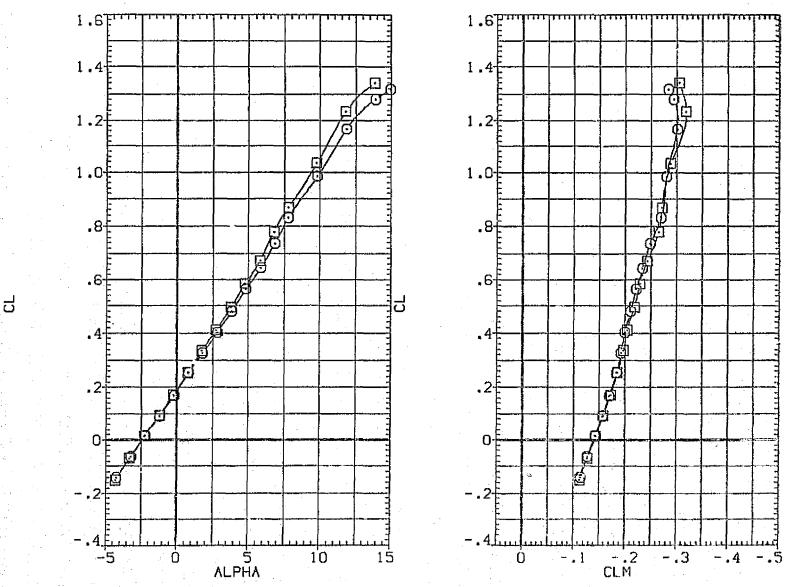


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET ON

(B)MACH = .90

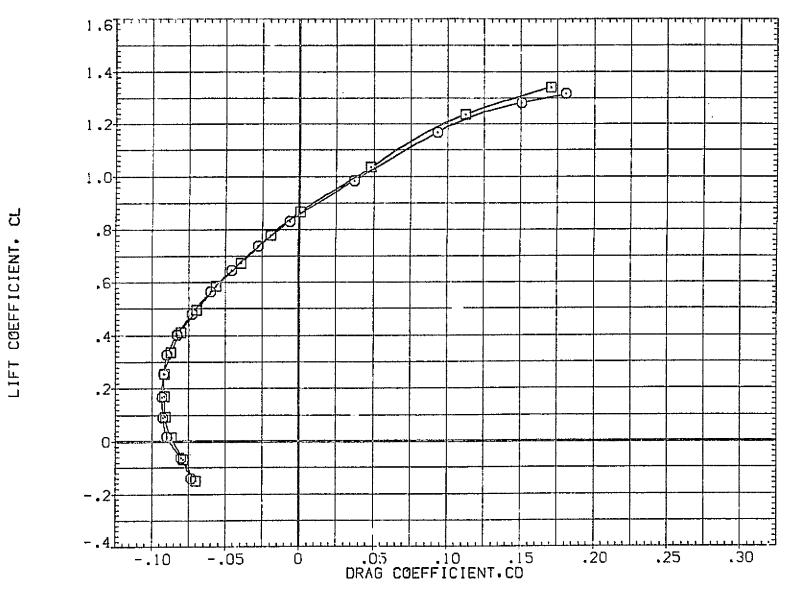


FIG. 12 REYNOLDS NUMBER SENSITIVITY WITH JET ON (B)MACH = .90

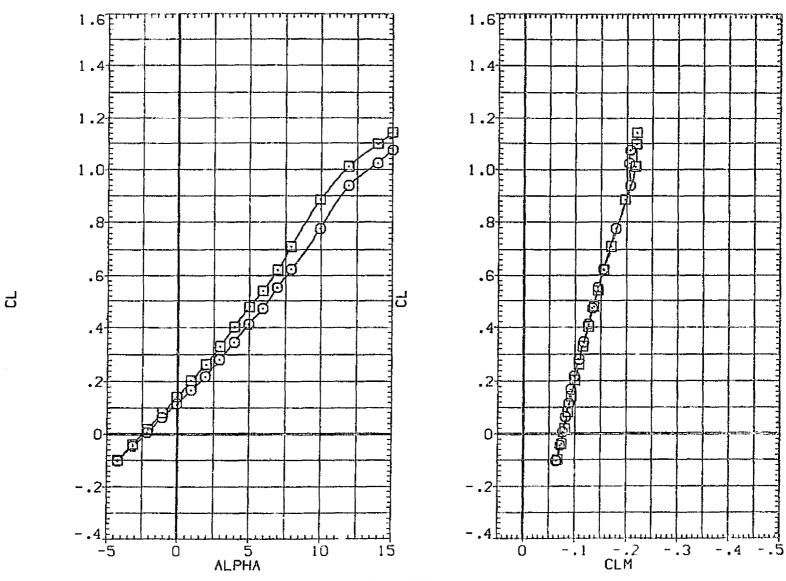


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2

(A)MACH = .70

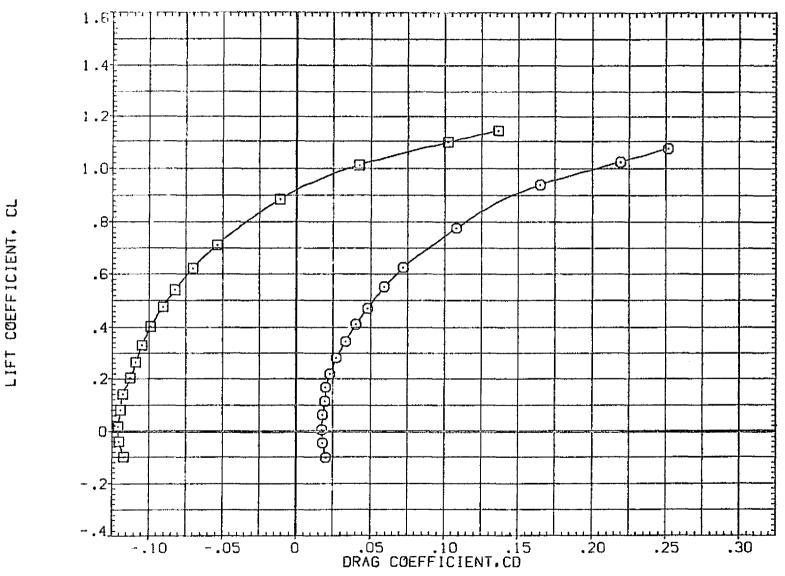


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2

(A)MACH = .70

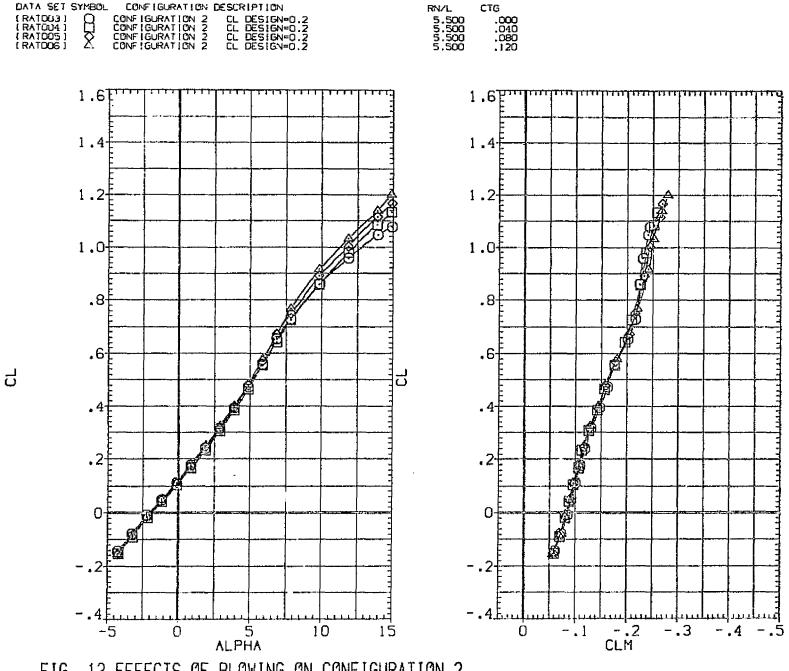


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2
(A)MACH = .90

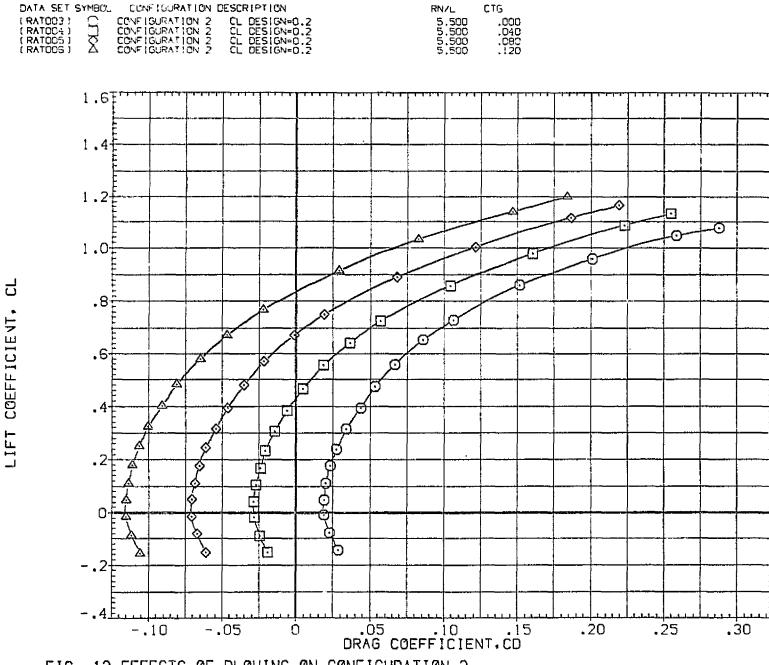


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2

(A)MACH = .90

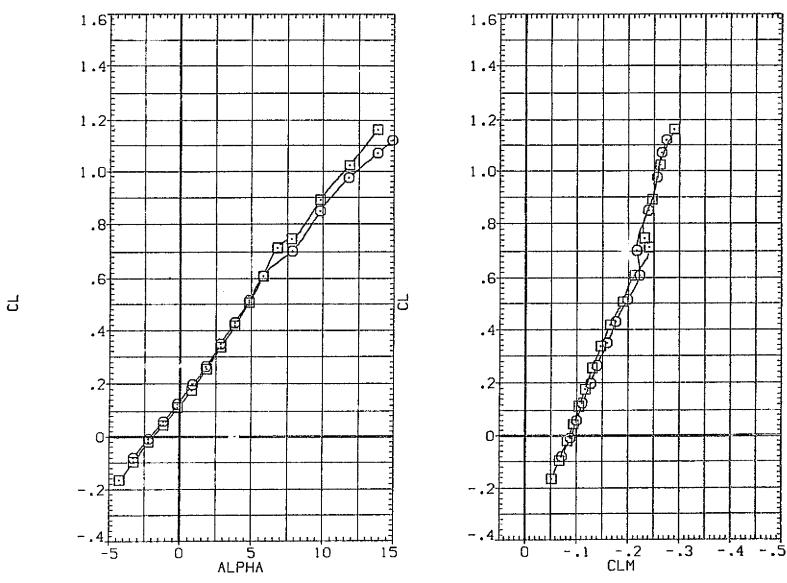


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2

(A)MACH = .95

COEFFICIENT,

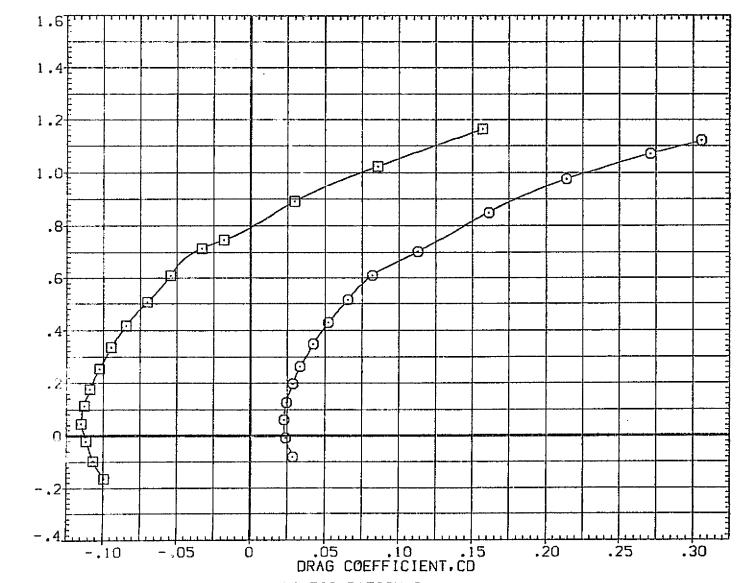


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 2

(A)MACH = .95

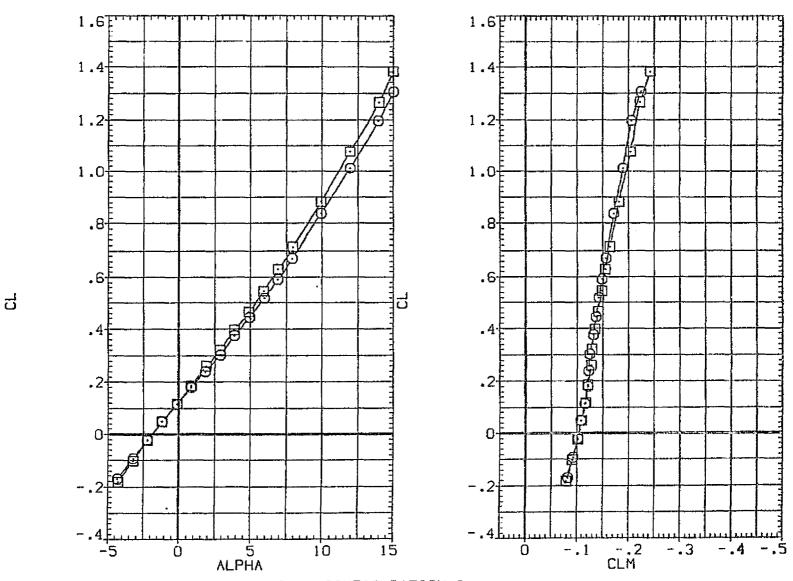


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3
(A)MACH = .70

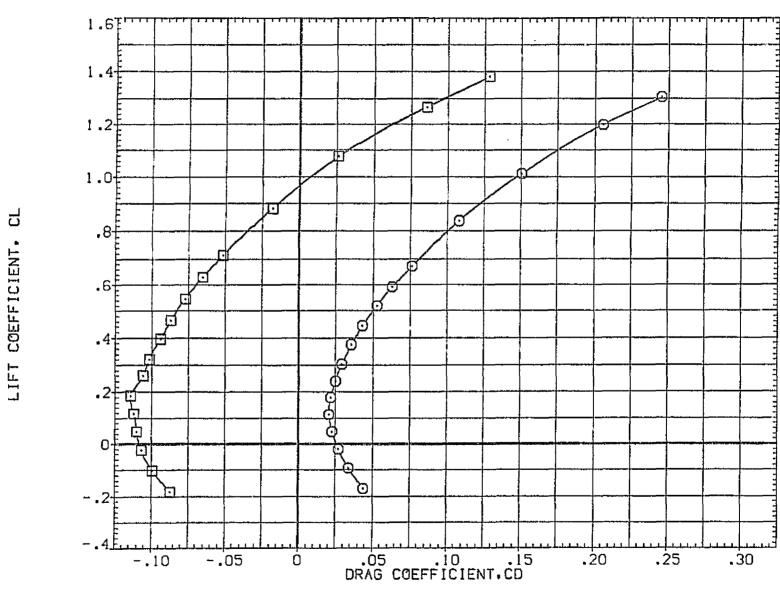


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3

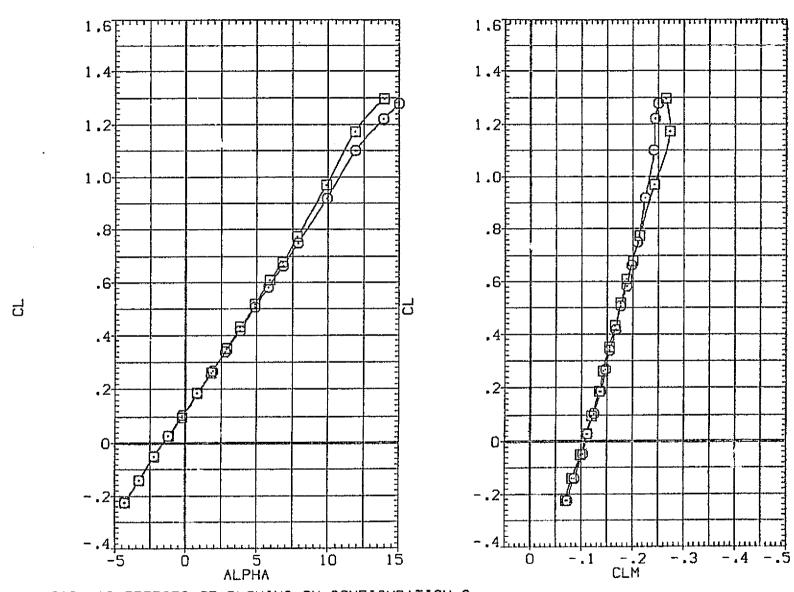


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3
(B)MACH = .90



FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3
(B)MACH = .90

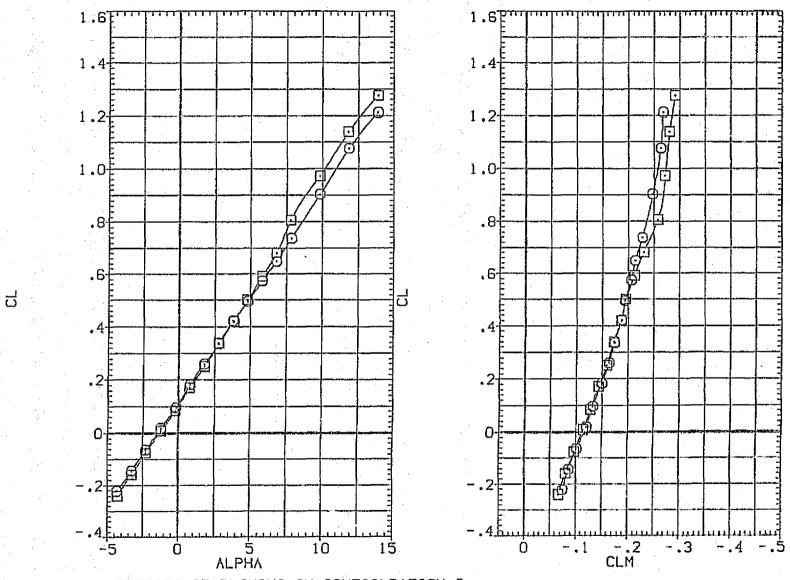


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3

COMACH = .95

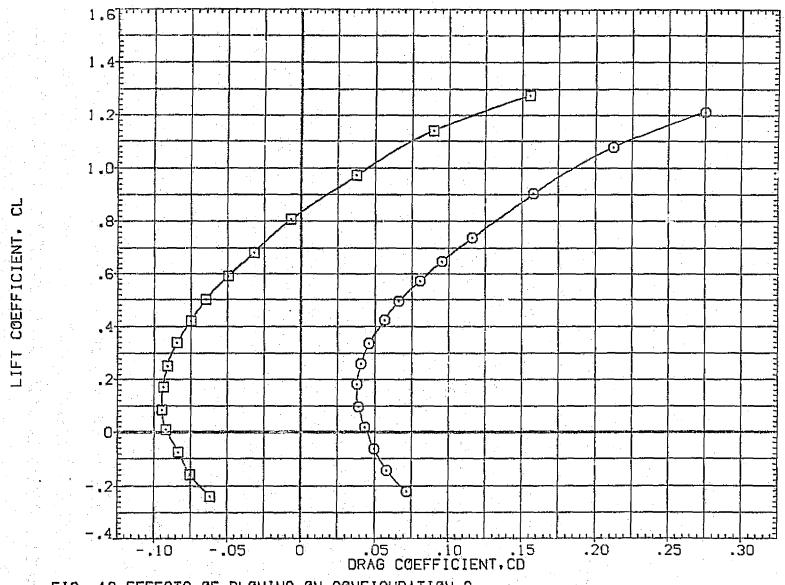


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 3
(C)MACH = .95

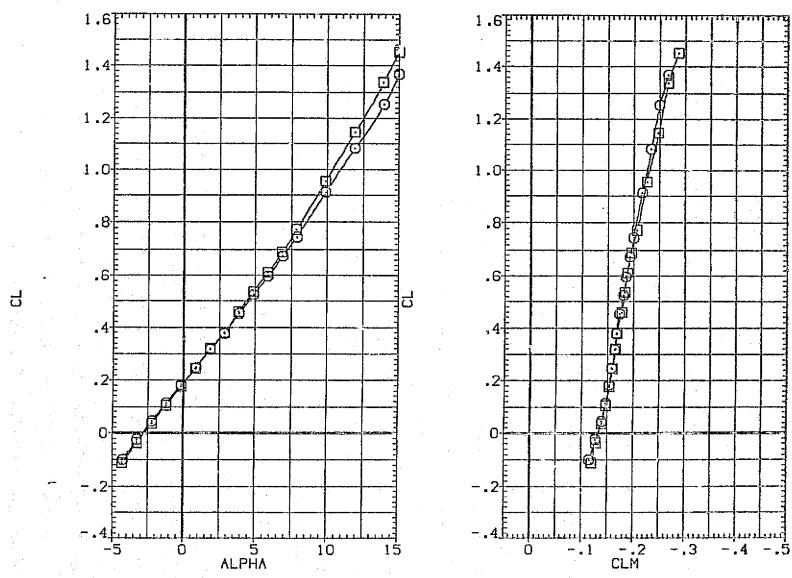


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4
(A)MACH = .70

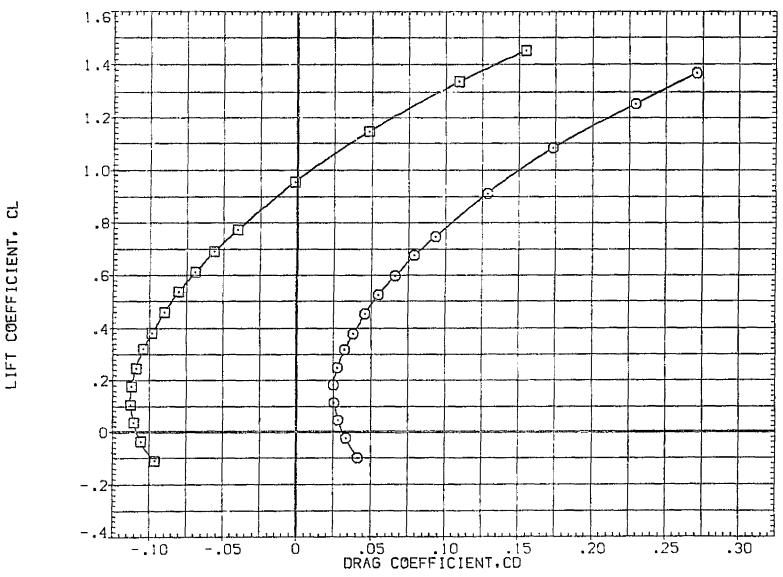


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4
(A)MACH = .70

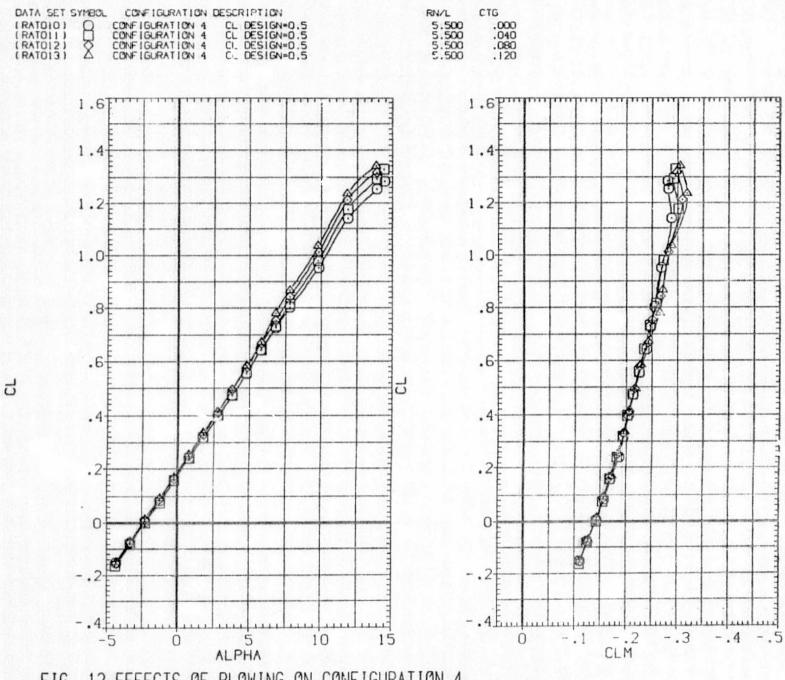


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4



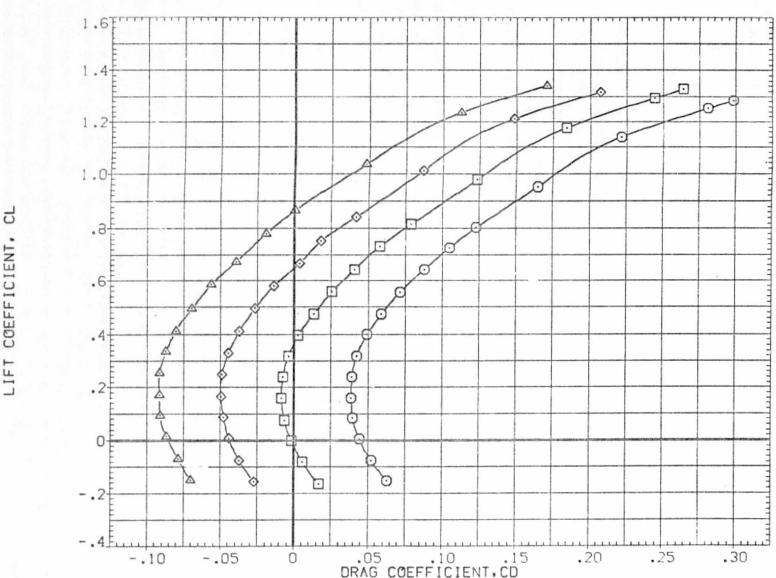


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4

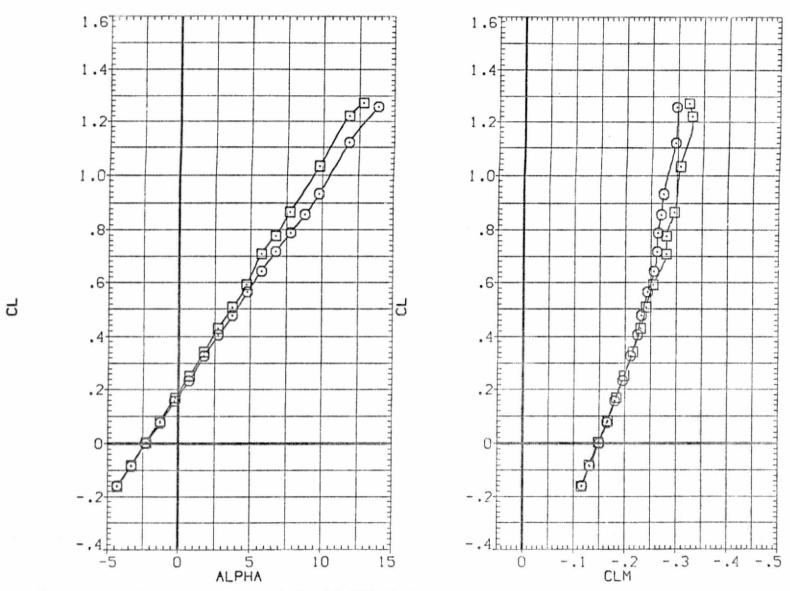


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4

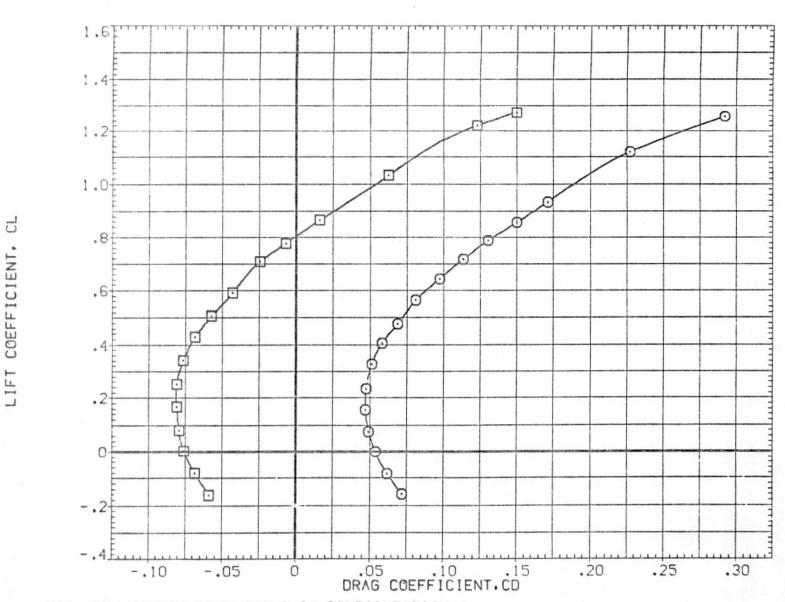
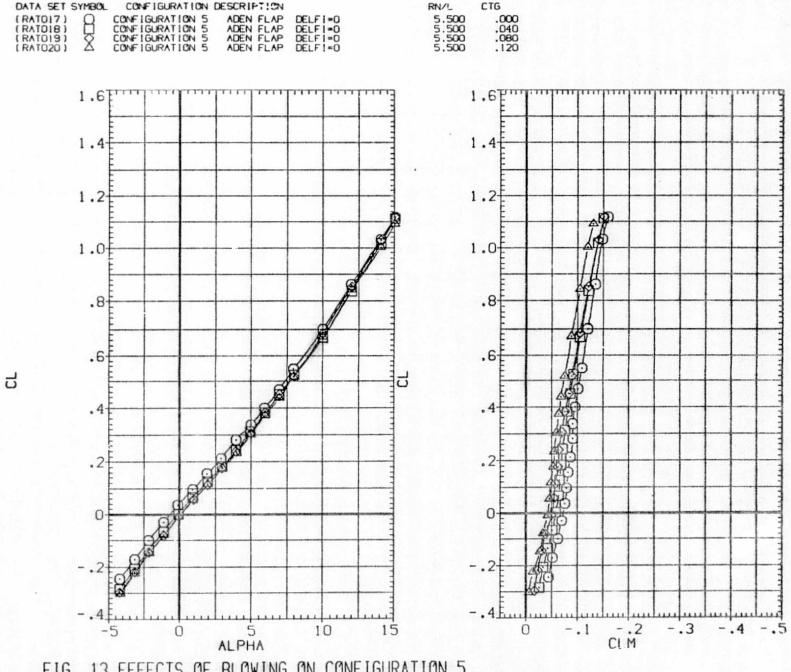


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 4



CTG

FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5 (A)MACH = .70

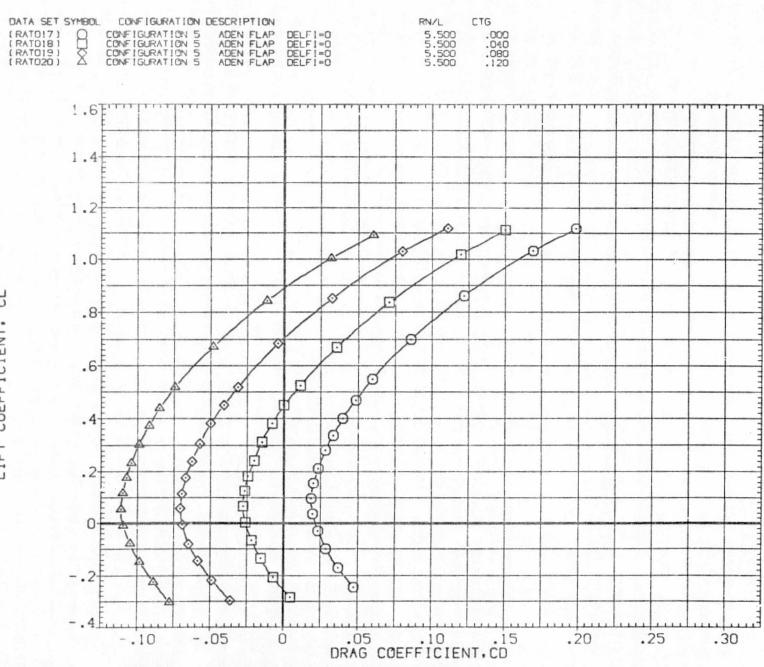


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5

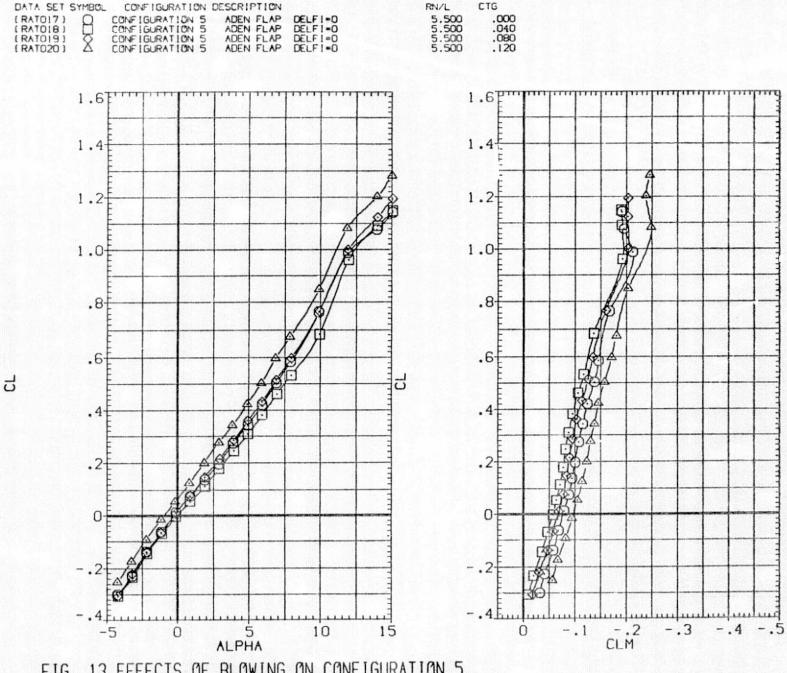


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5
(B)MACH = .90





FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5
(B)MACH = .90

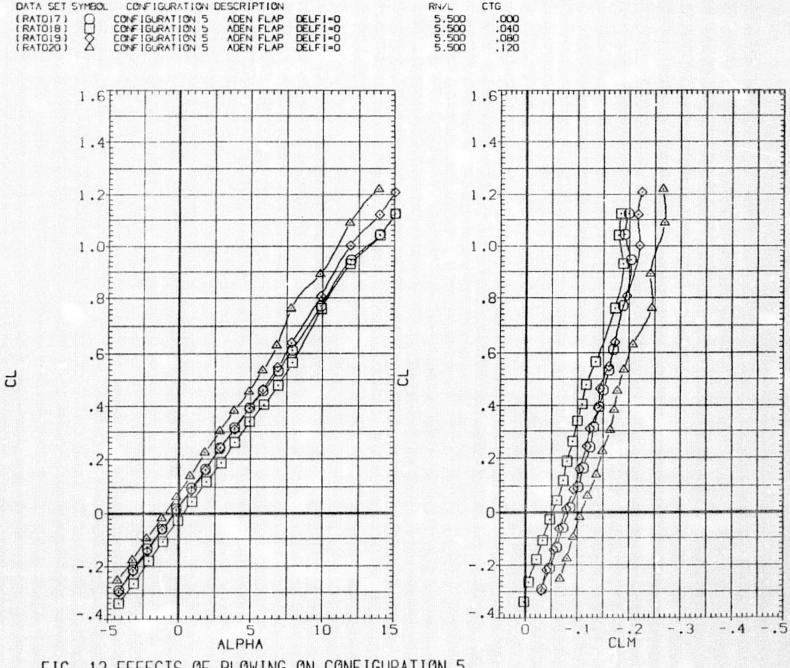


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5

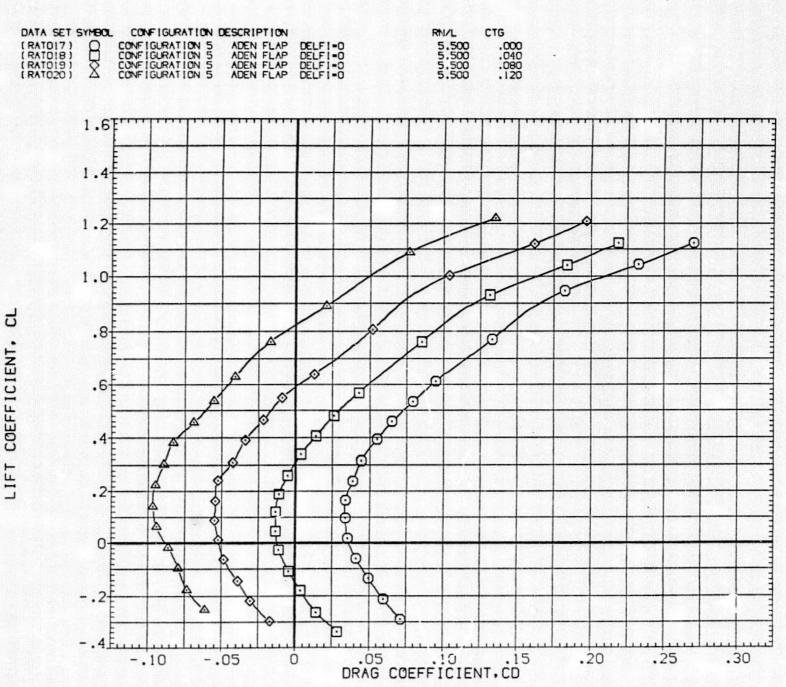


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 5

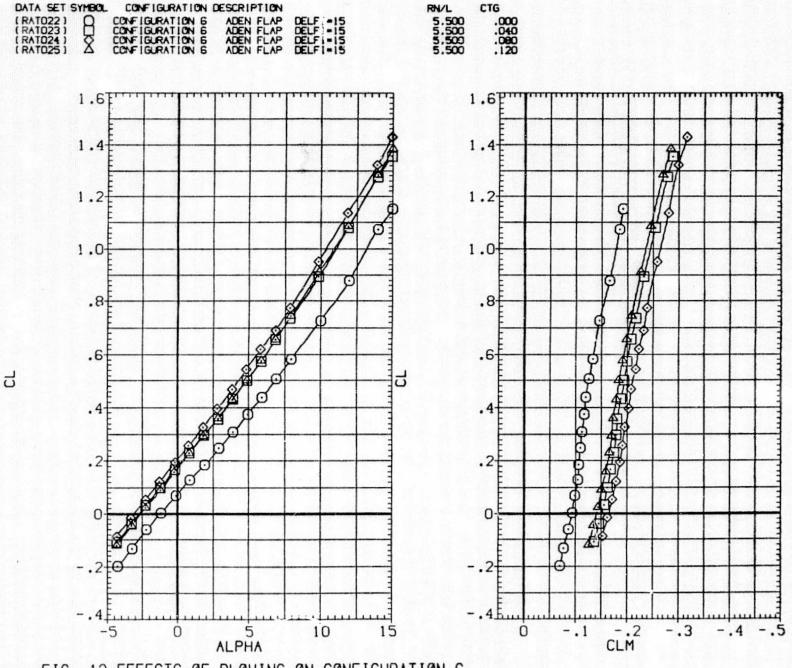


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 6

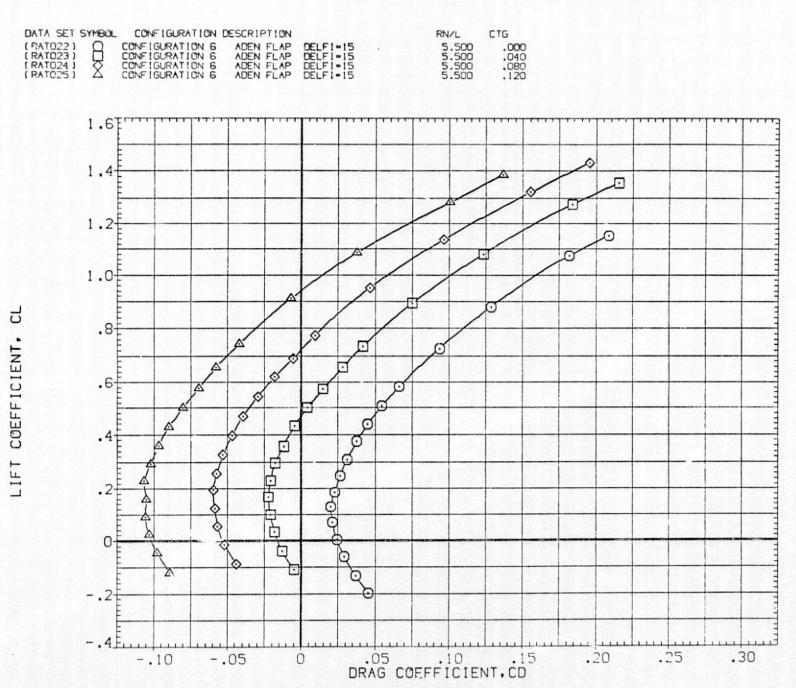
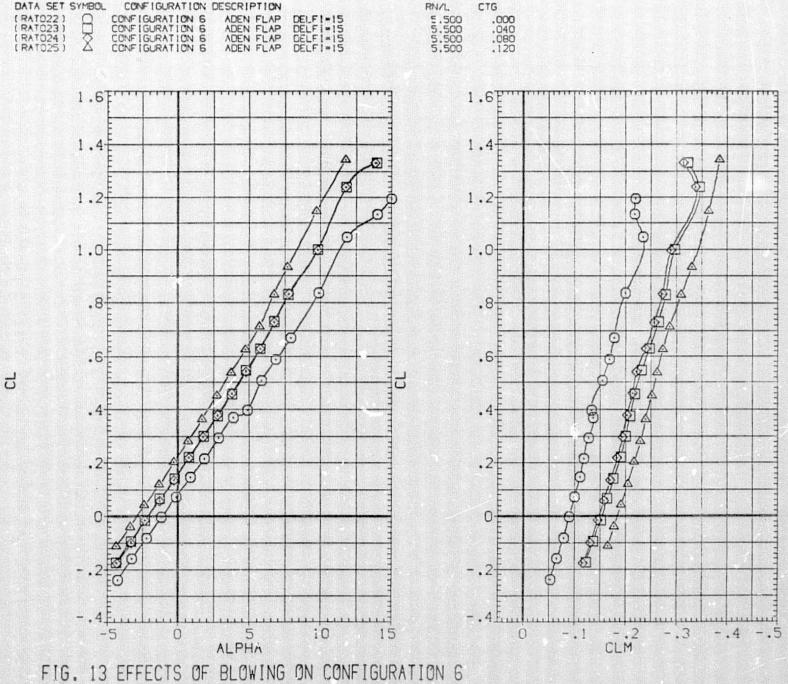


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 6

PAGE



(B)MACH .90 =

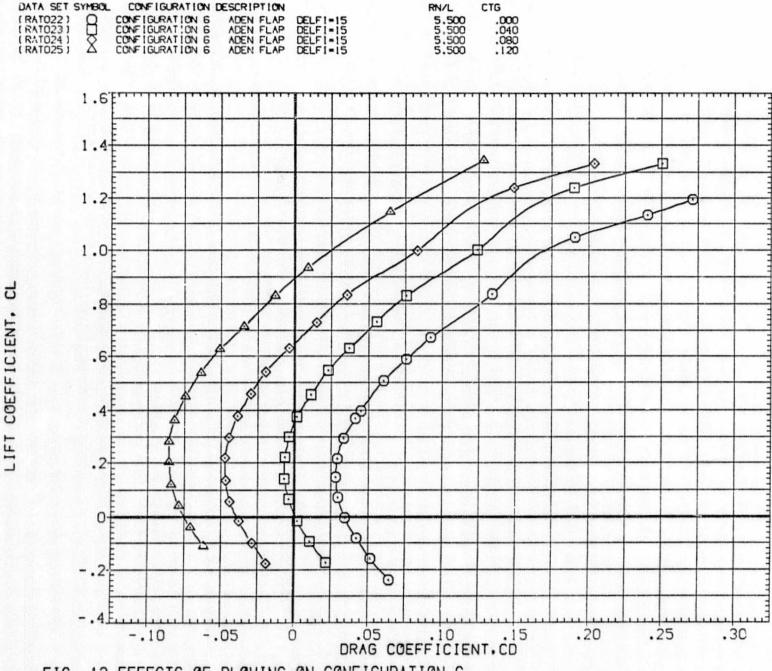


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 6
(B)MACH = .90

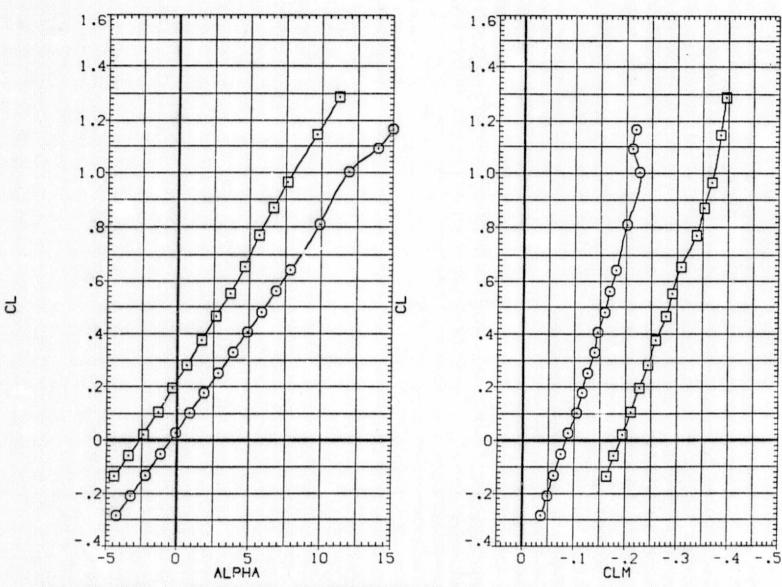


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 6

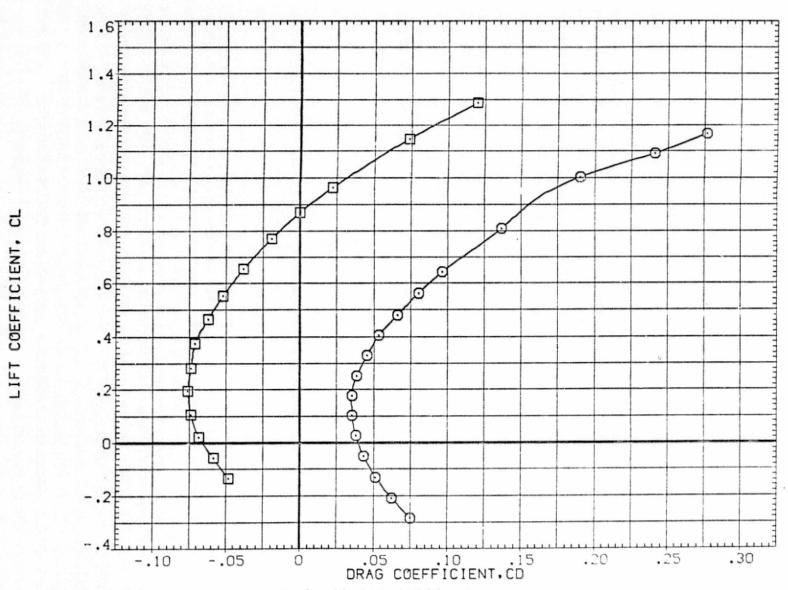


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 6

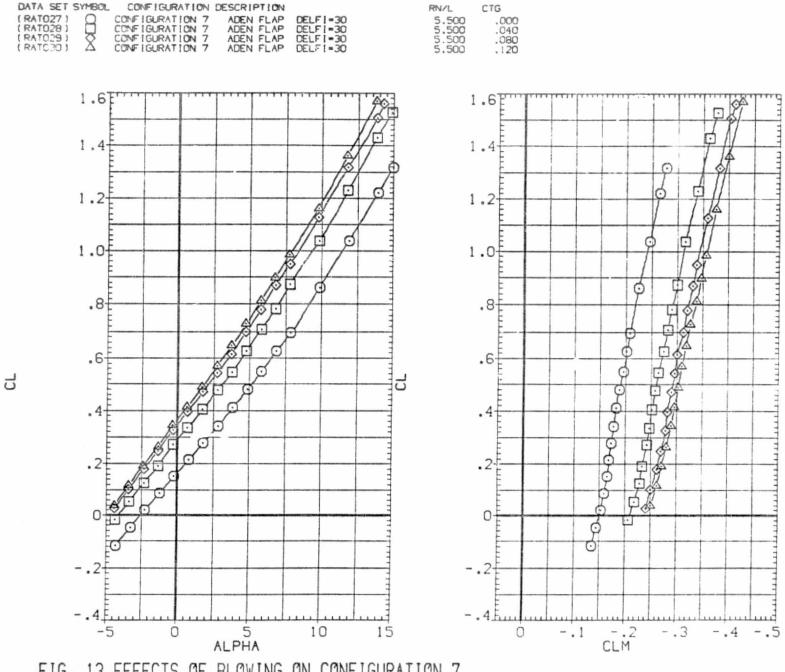


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 7



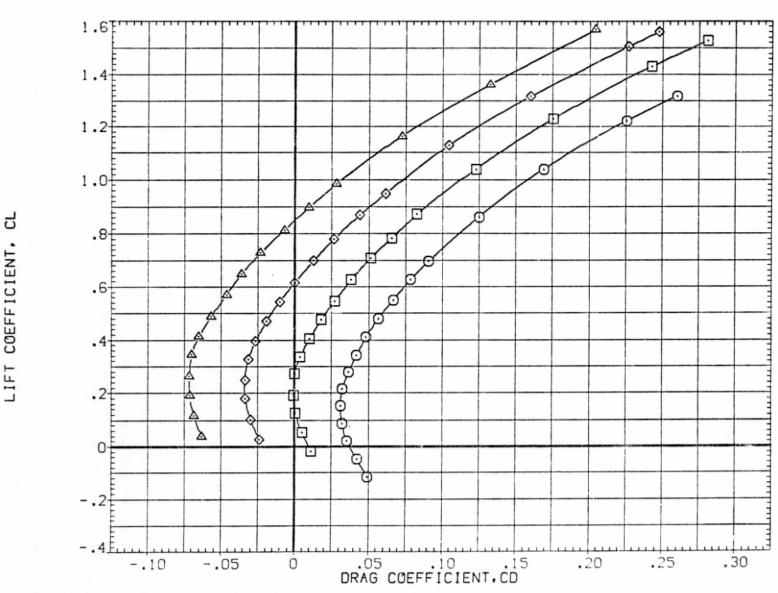


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 7

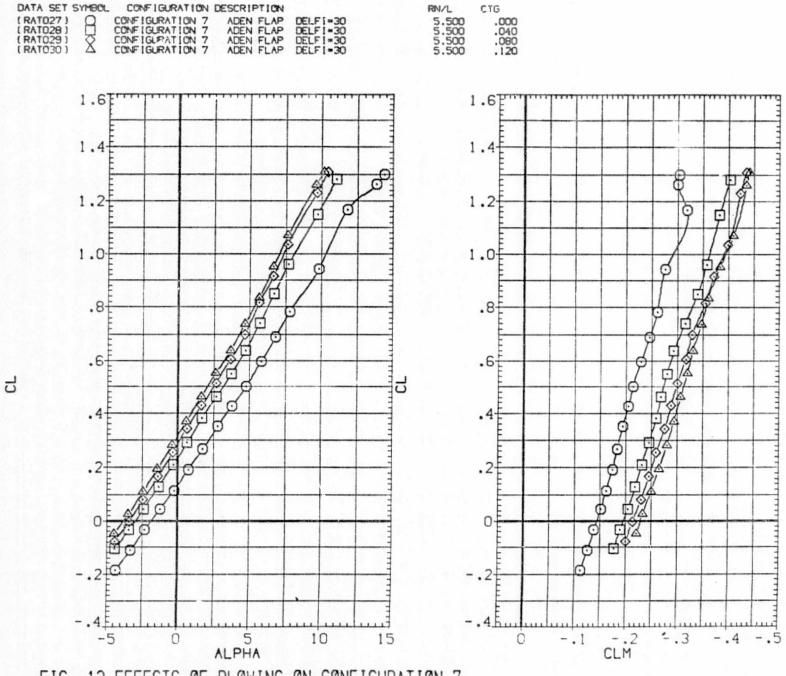
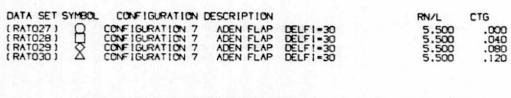


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 7
(B)MACH = .90



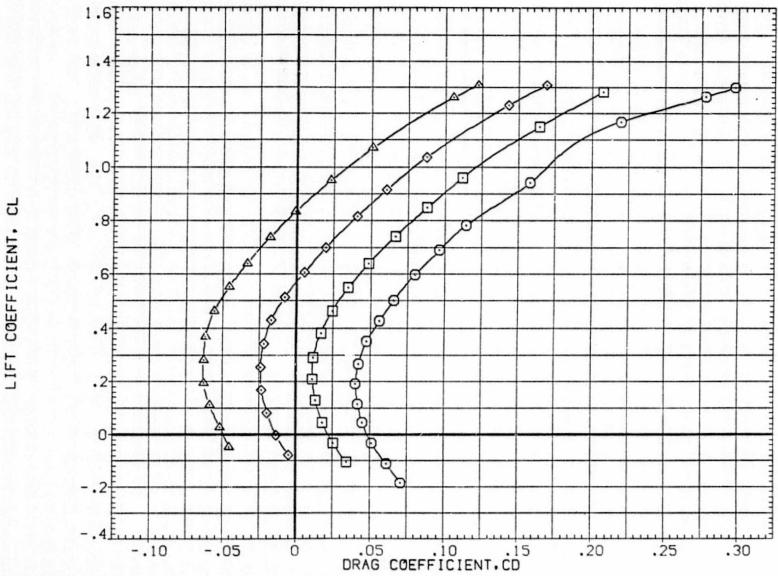
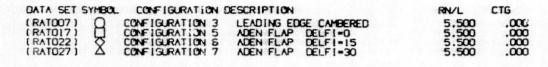
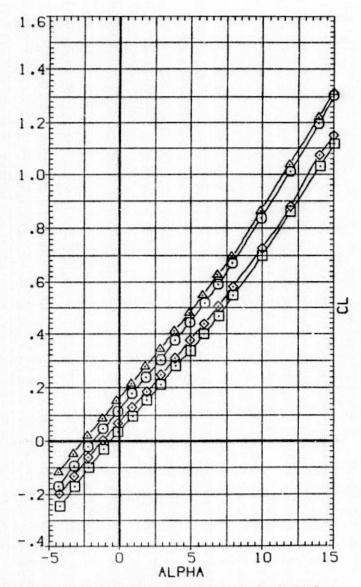


FIG. 13 EFFECTS OF BLOWING ON CONFIGURATION 7

(B)MACH = .90

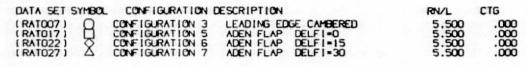




1.67 1.4 1.2 1.0 B .8+ .6 A .2 0 CLM -.3 -.4 -.5 Ó -.1

FIG. 14 FLAP EFFECTS WITH NO BLOWING

(A)MACH = .70



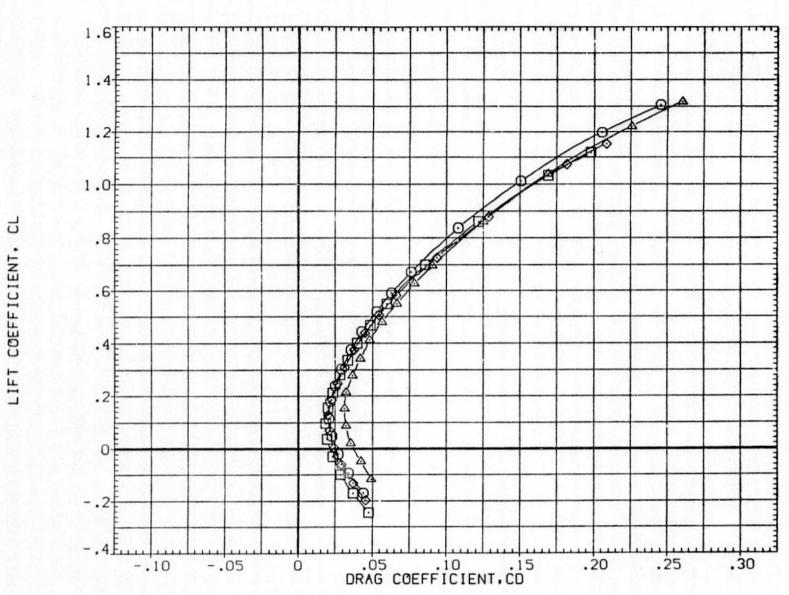
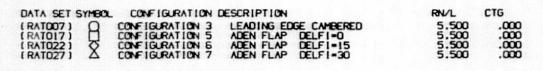
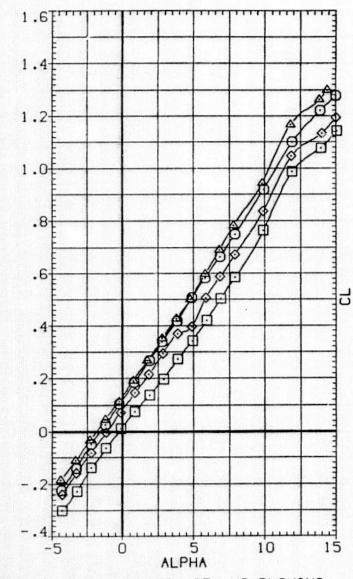


FIG. 14 FLAP EFFECTS WITH NO BLOWING





1.67 1.4 1.2 A 1.0 .8 þ .6 0 CLM -.3 0

FIG. 14 FLAP EFFECTS WITH NO BLOWING
(B)MACH = .90



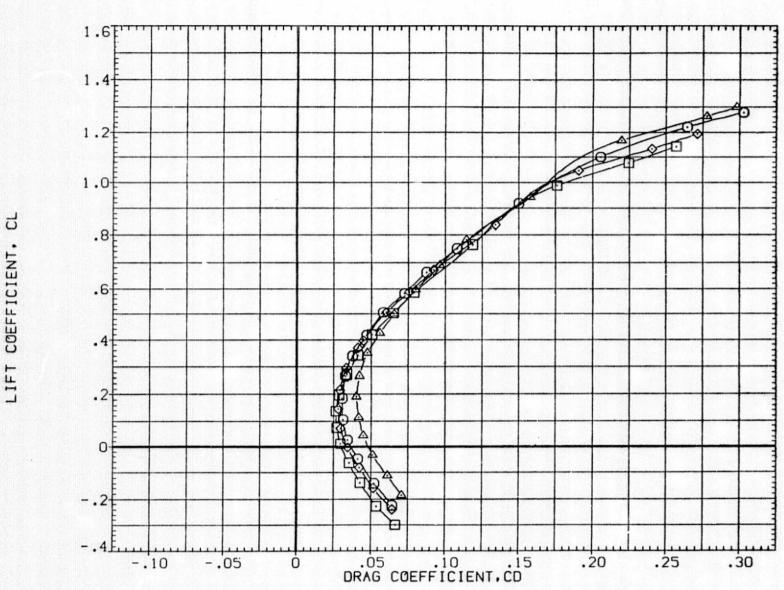
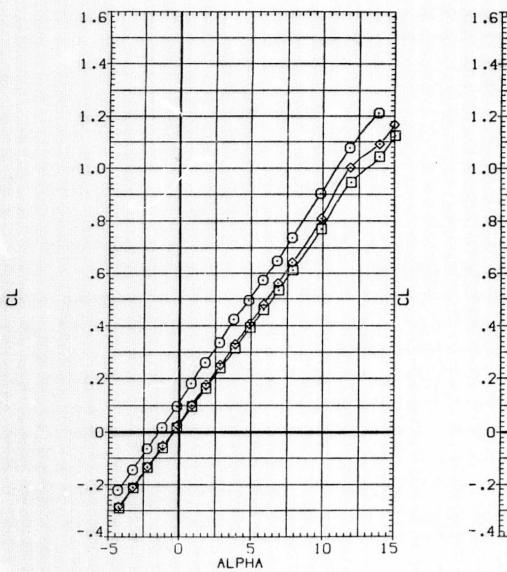


FIG. 14 FLAP EFFECTS WITH NO BLOWING





1.67 Q 0 -.2 -.3 -.4 -.5 CLM

FIG. 14 FLAP EFFECTS WITH NO BLOWING

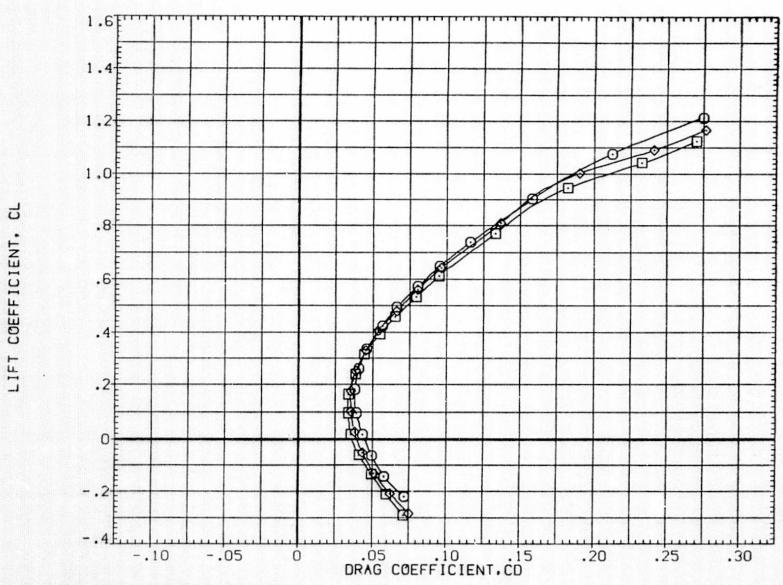
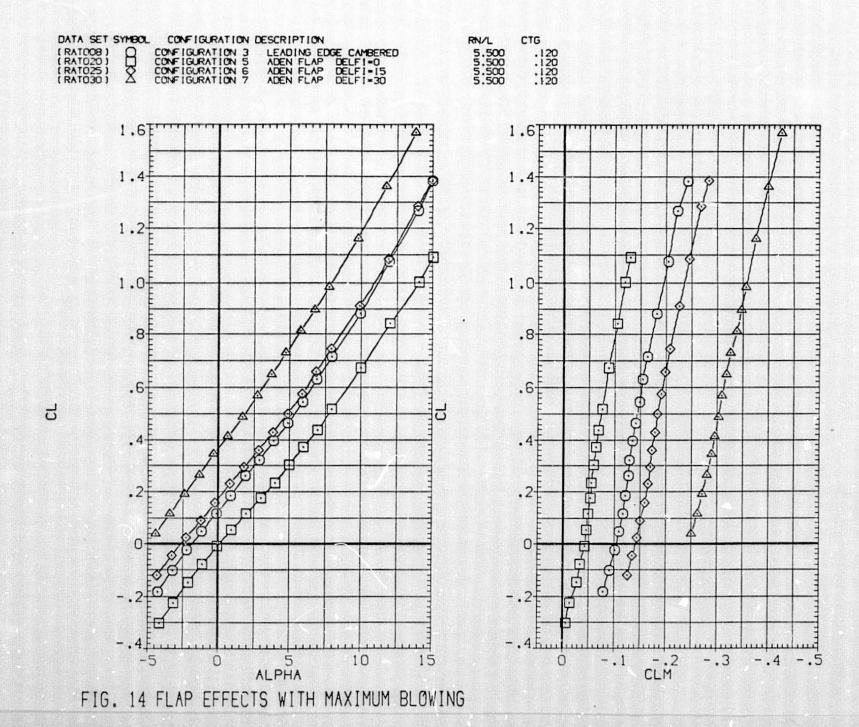


FIG. 14 FLAP EFFECTS WITH NO BLOWING





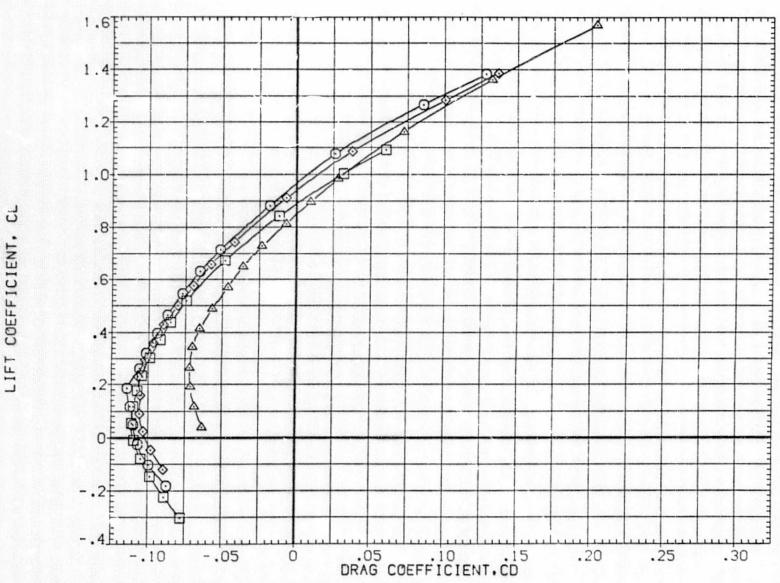


FIG. 14 FLAP EFFECTS WITH MAXIMUM BLOWING

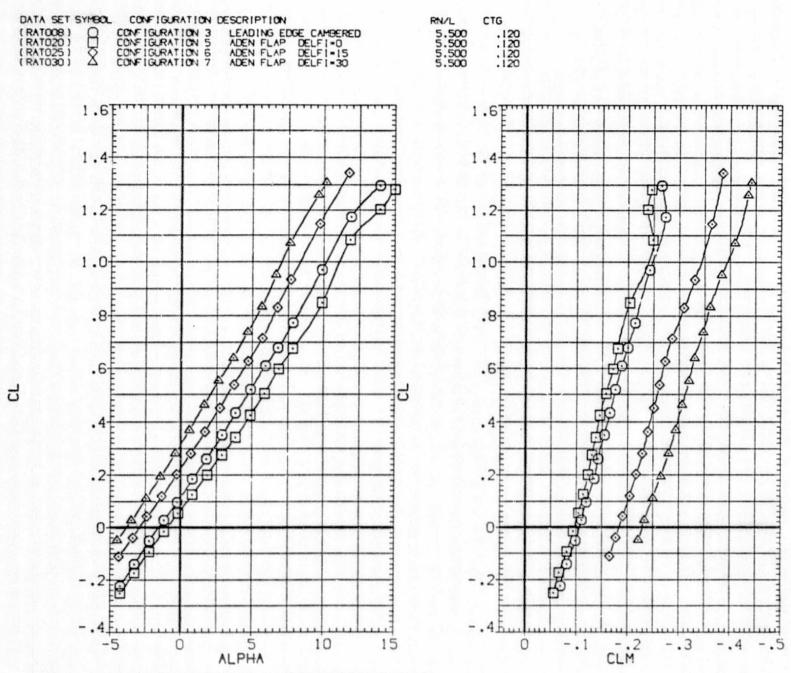


FIG. 14 FLAP EFFECTS WITH MAXIMUM BLOWING
(B)MACH = .90



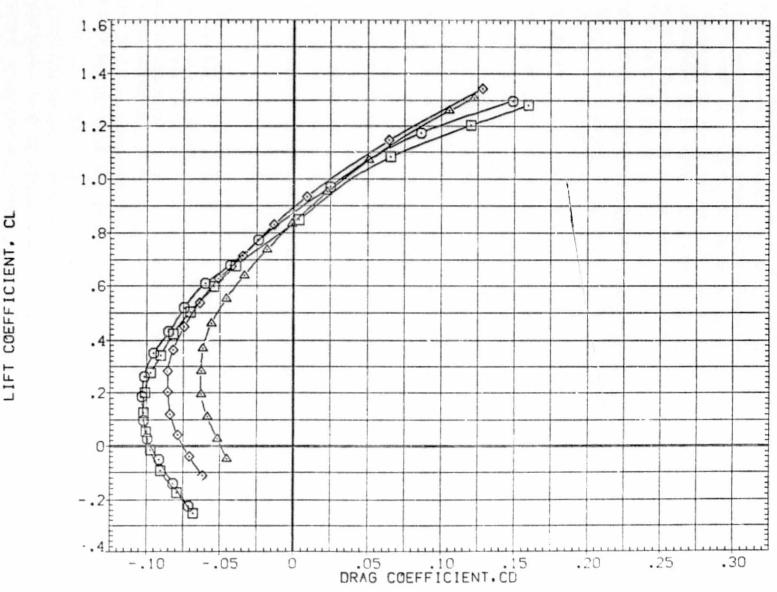
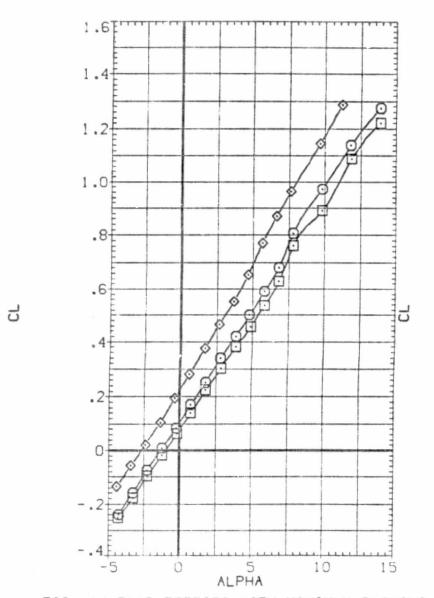


FIG. 14 FLAP EFFECTS WITH MAXIMUM BLOWING





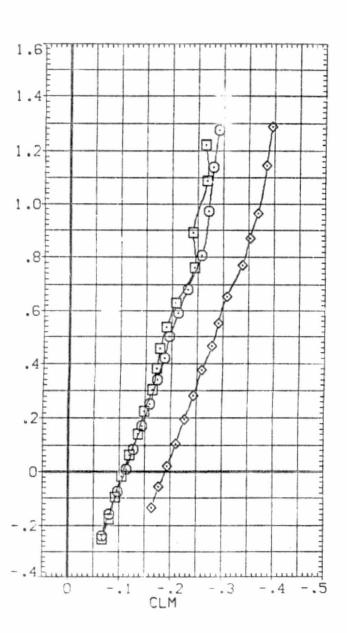


FIG. 14 FLAP EFFECTS WITH MAXIMUM BLOWING
(A)MACH = .95



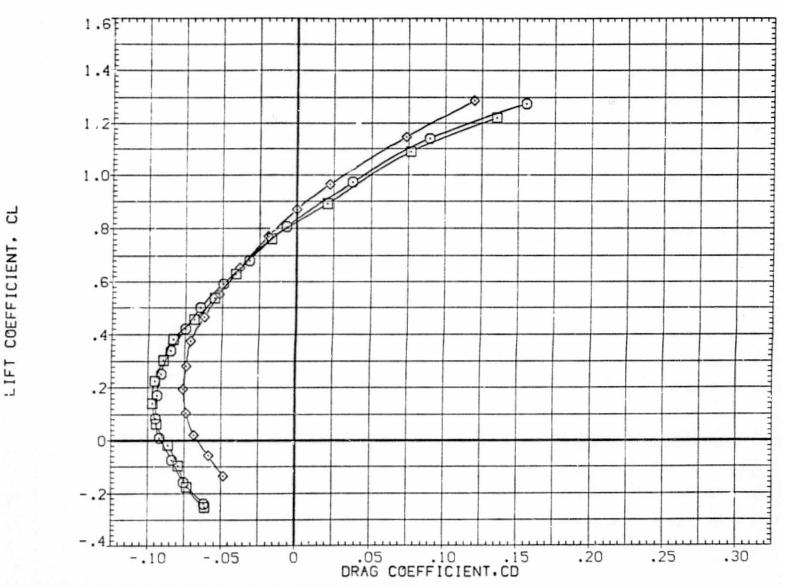
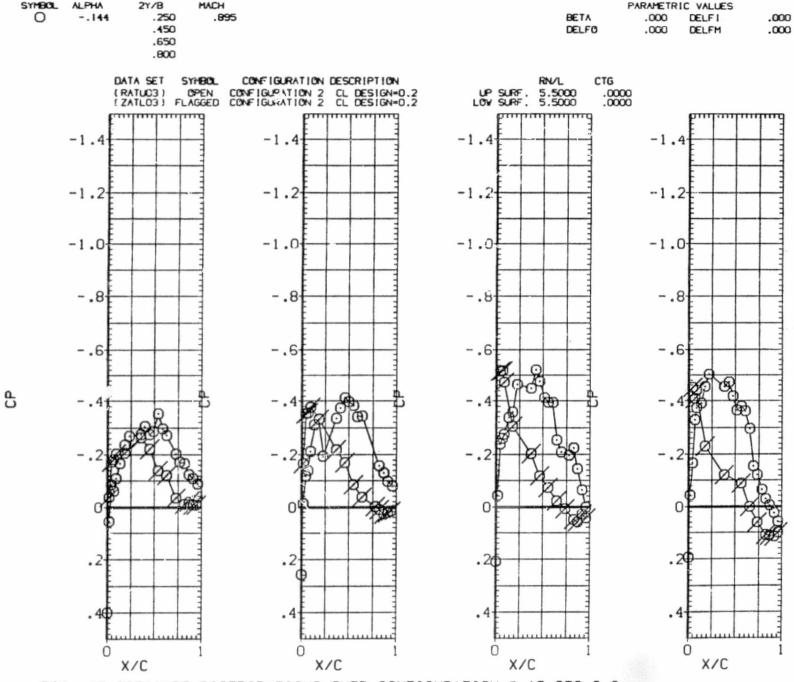


FIG. 14 FLAP EFFECTS WITH MAXIMUM BLOWING
(A)MACH = .95



2Y/B

MACH

FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.0

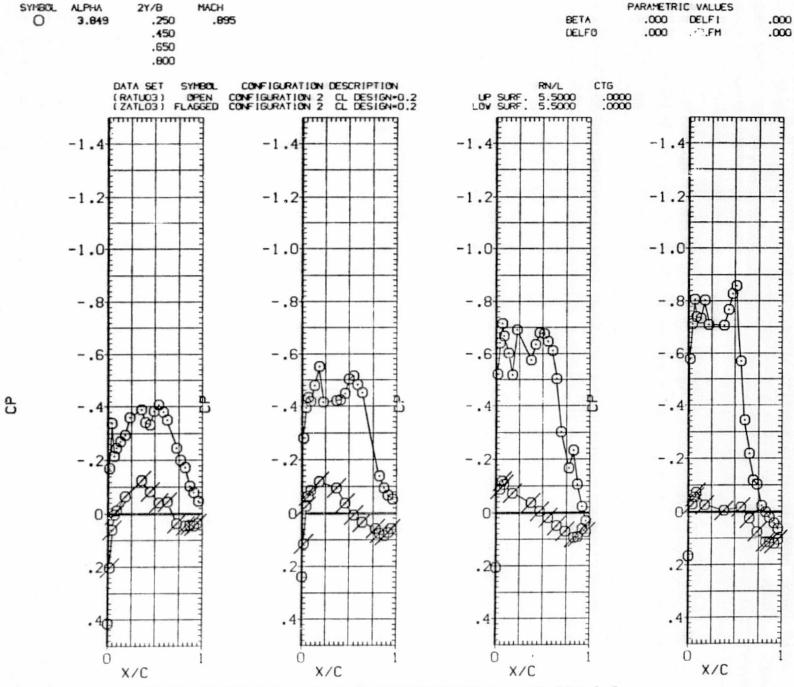


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.0

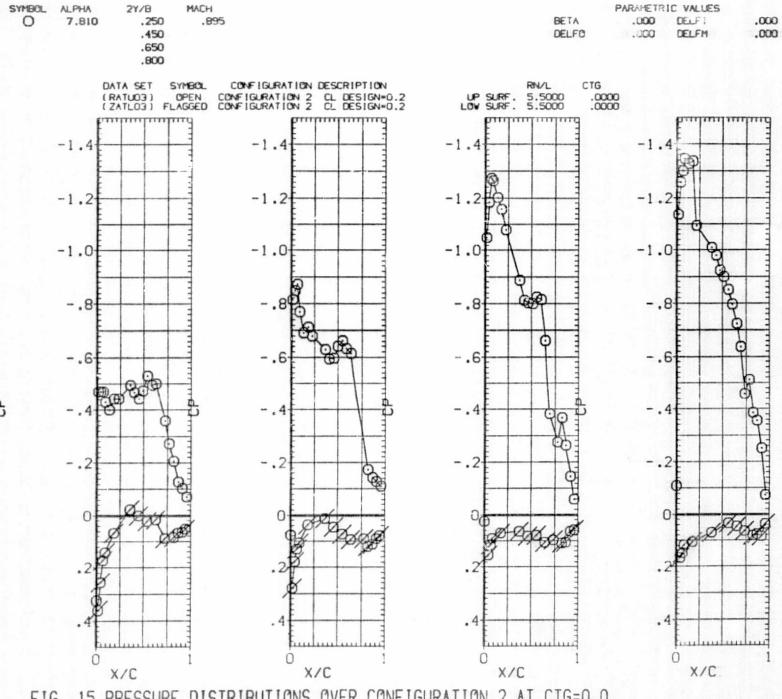
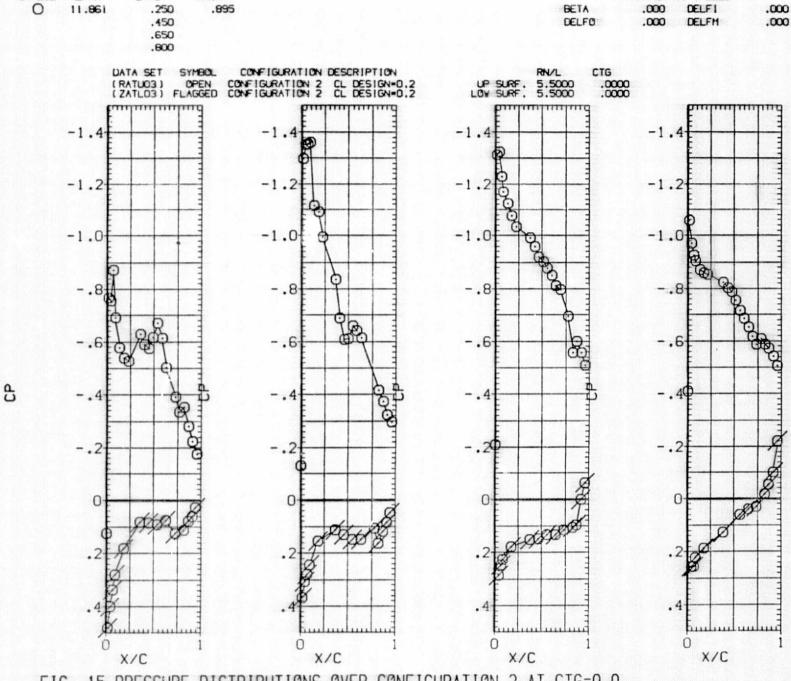


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.0



MACH

2Y/B

SYMBOL

ALPHA

FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.0

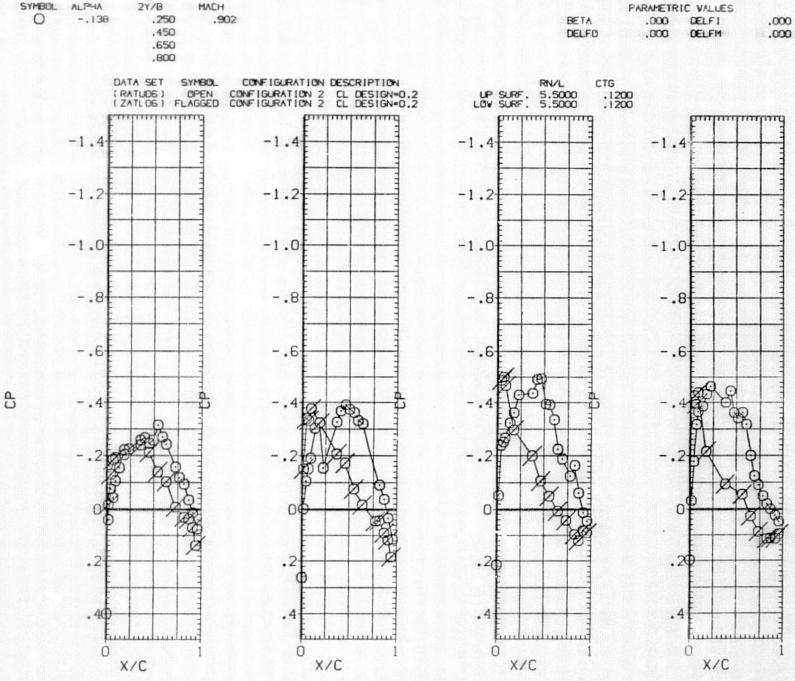


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.12

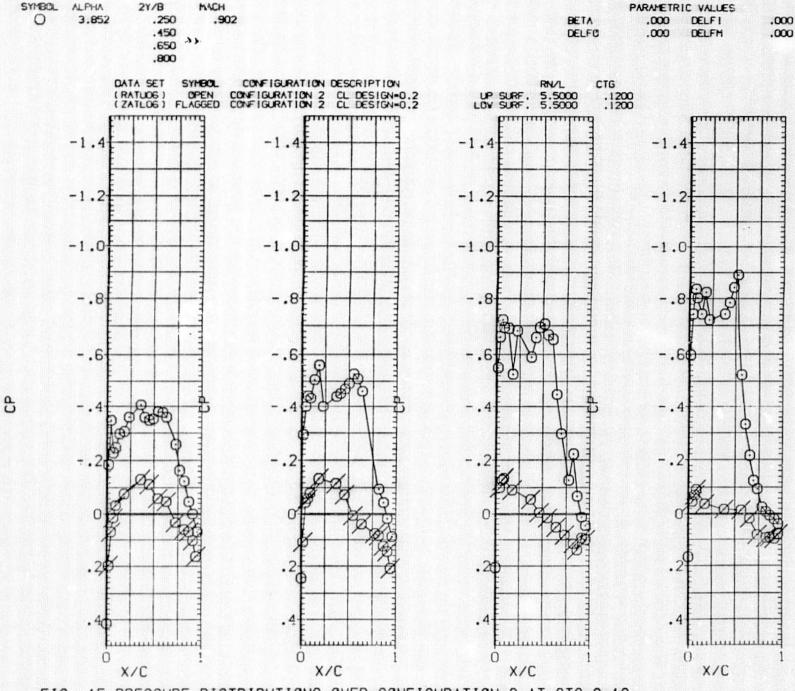


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.12

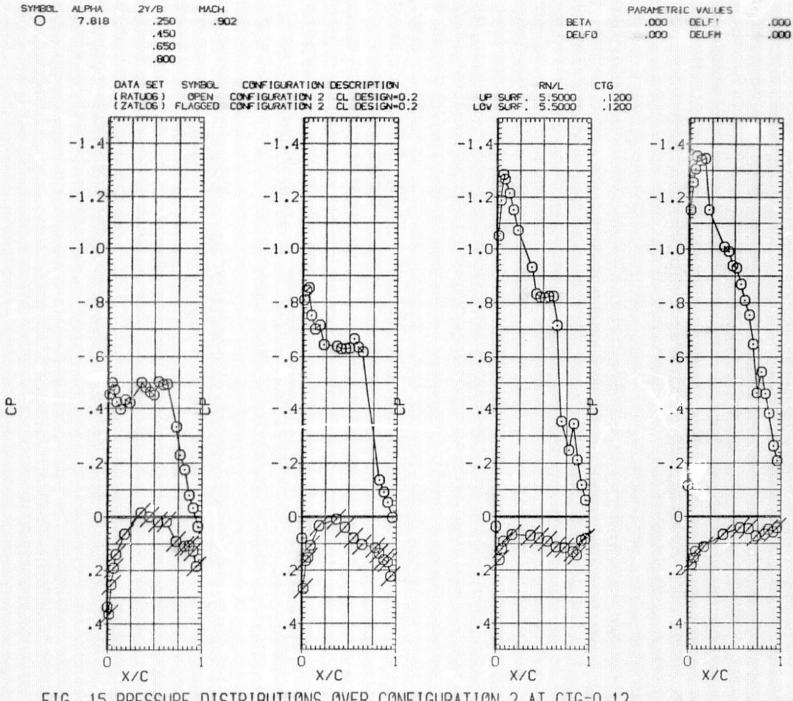


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.12

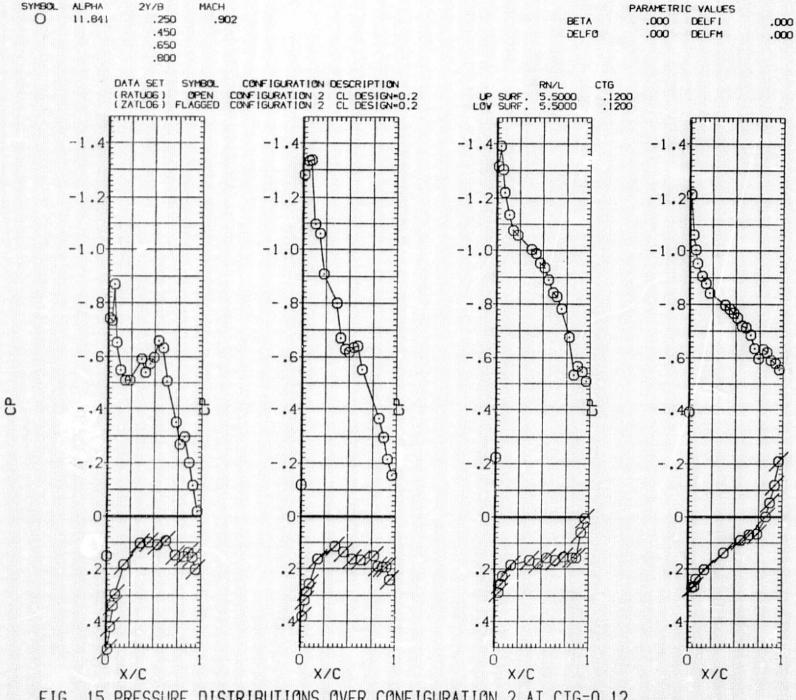
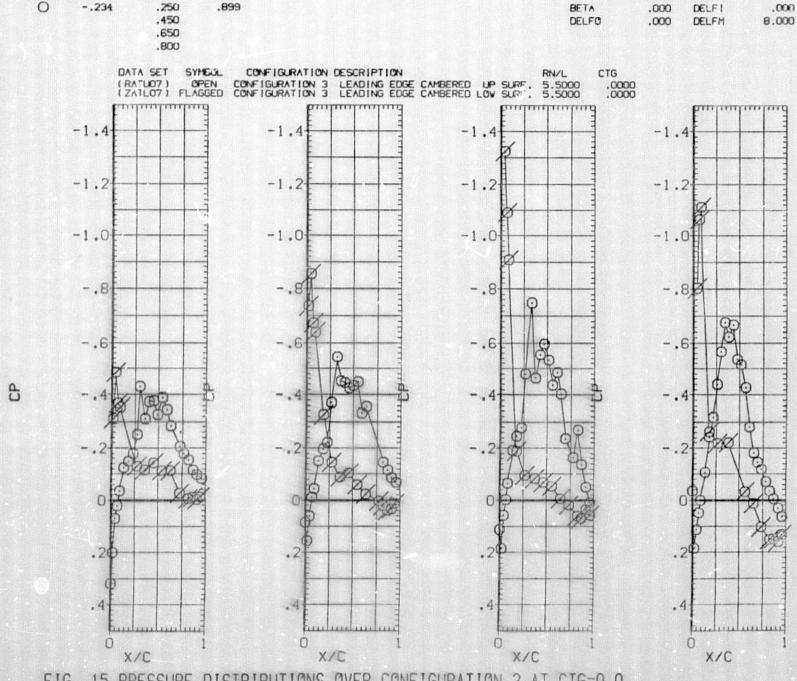


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 2 AT CTG=0.12



MACH

.899

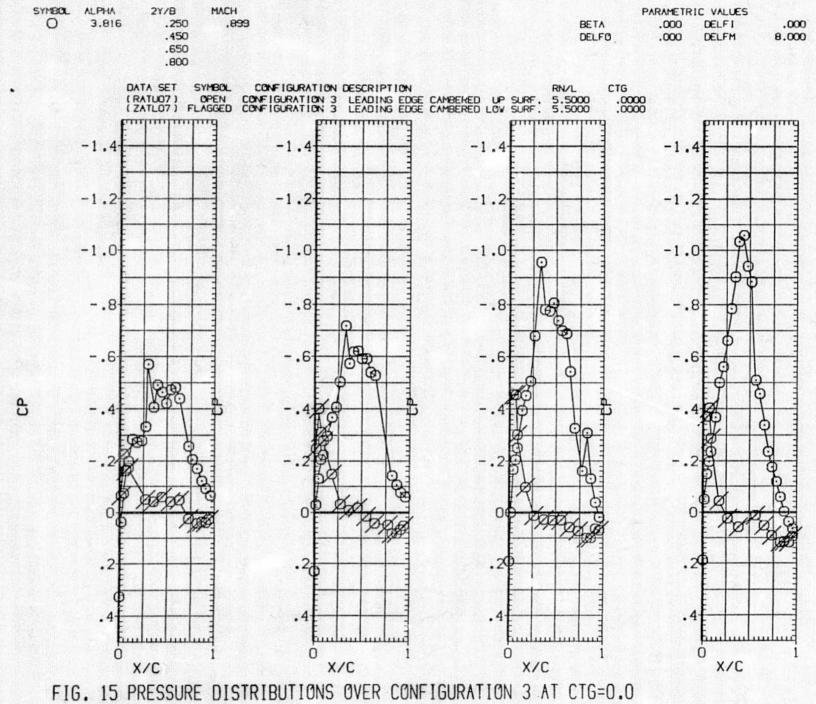
2Y/B

.250

SYMBOL

ALPHA

FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 3 AT CTG=0.0



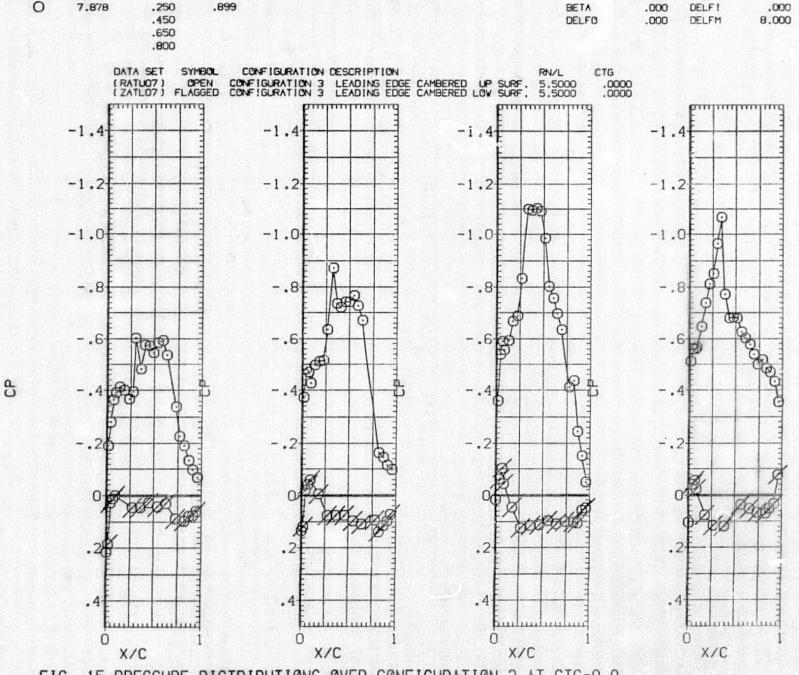


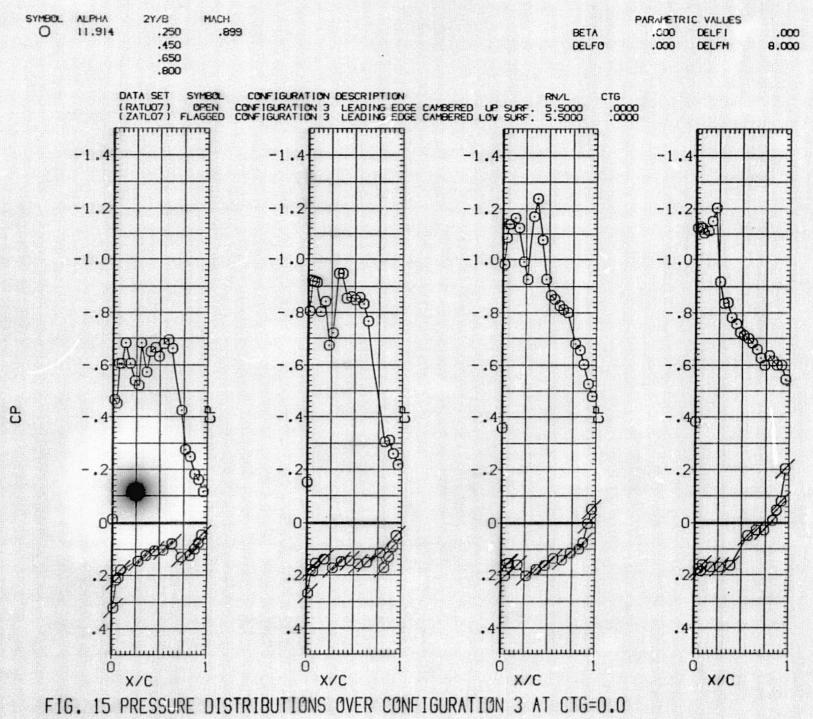
FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 3 AT CTG=0.0

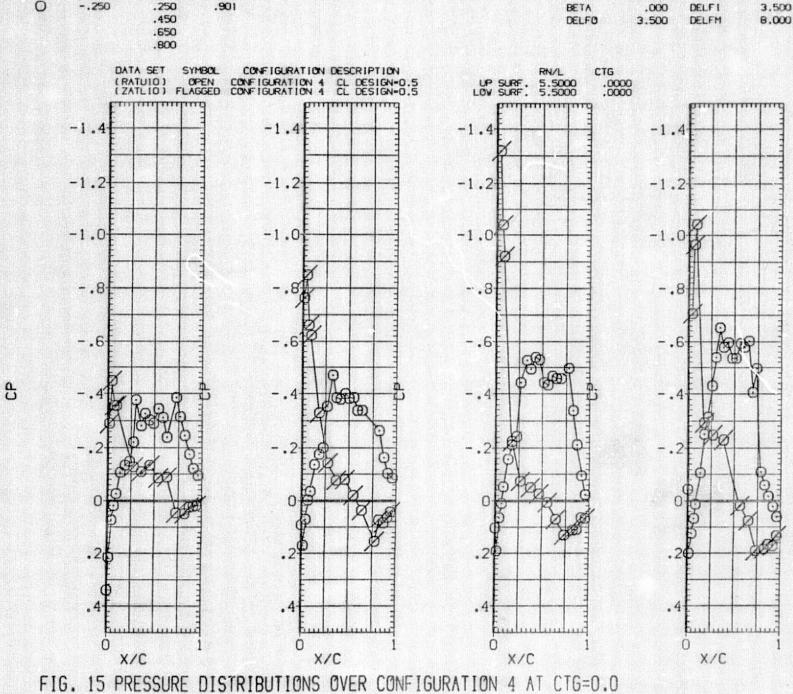
SYMBOL

ALPHA

MACH

2Y/B



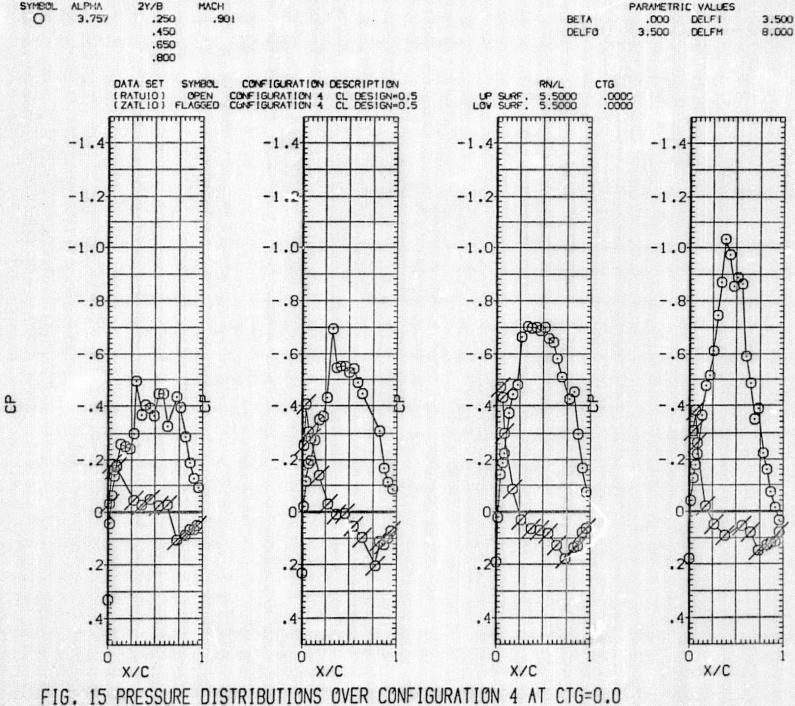


SYMBOL

ALPHA

2Y/B

MACH



ALPHA

2Y/B

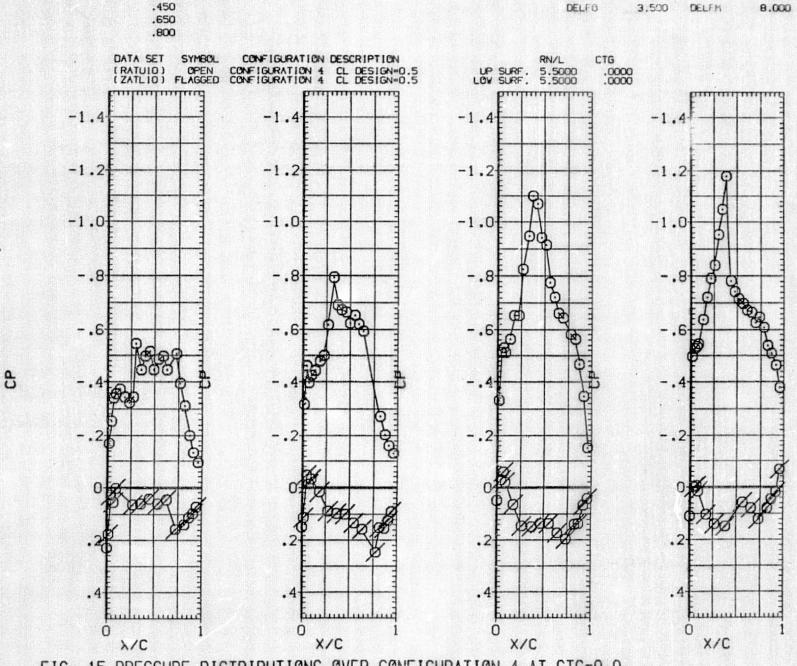


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 4 AT CTG=0.0

SYMBOL

0

ALPHA

7.776

2Y/B

.250

MACH

.901

PARAMETRIC VALUES

DEL.

3.500

BETA

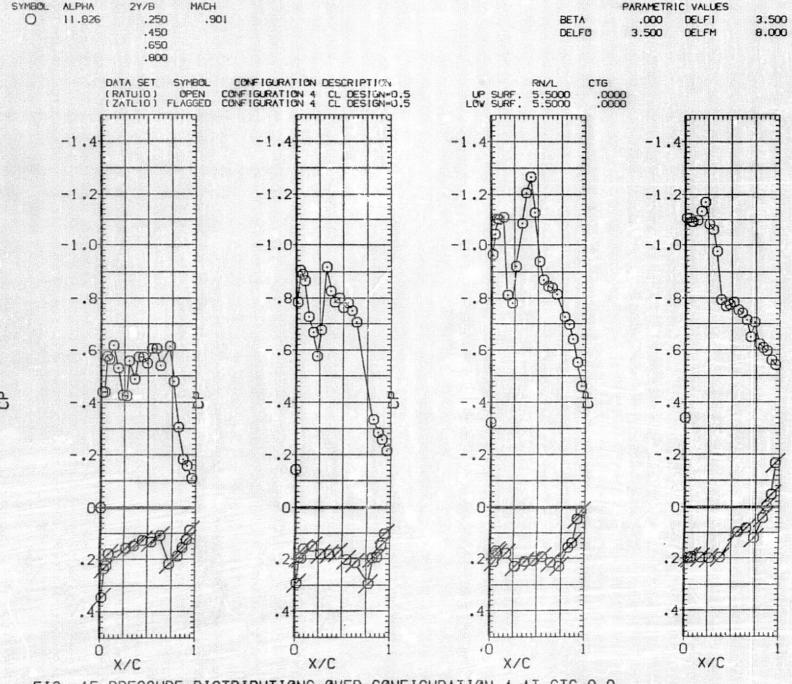
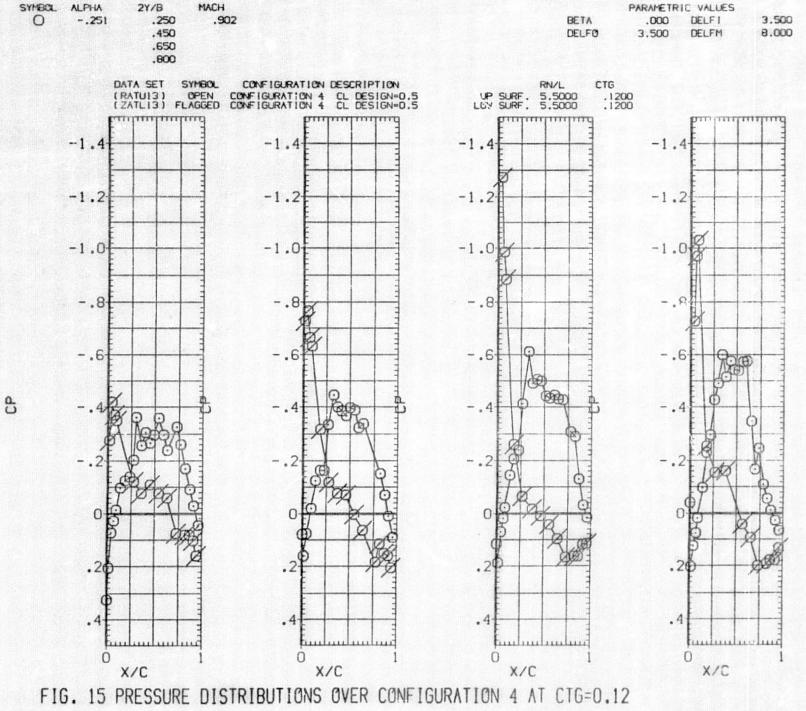
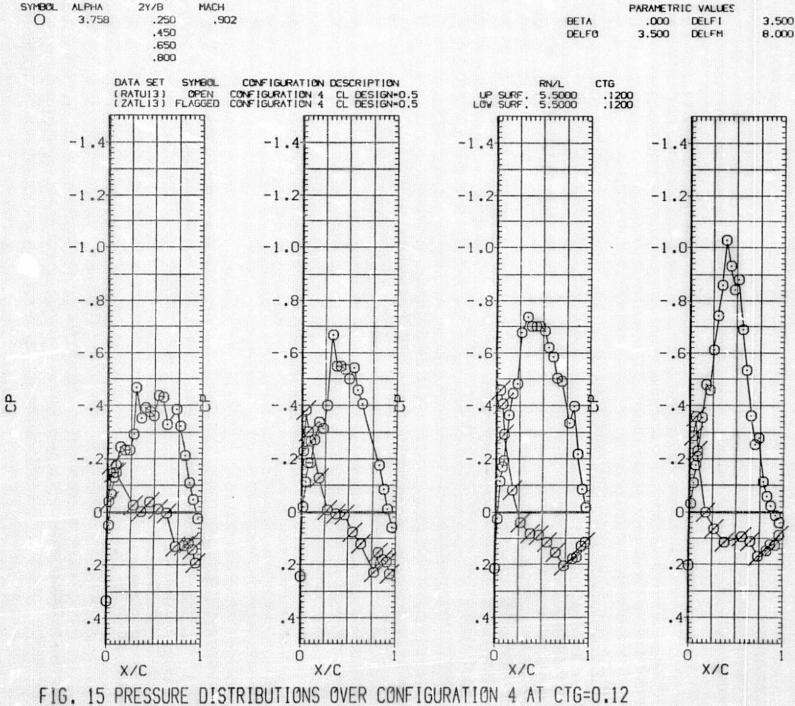
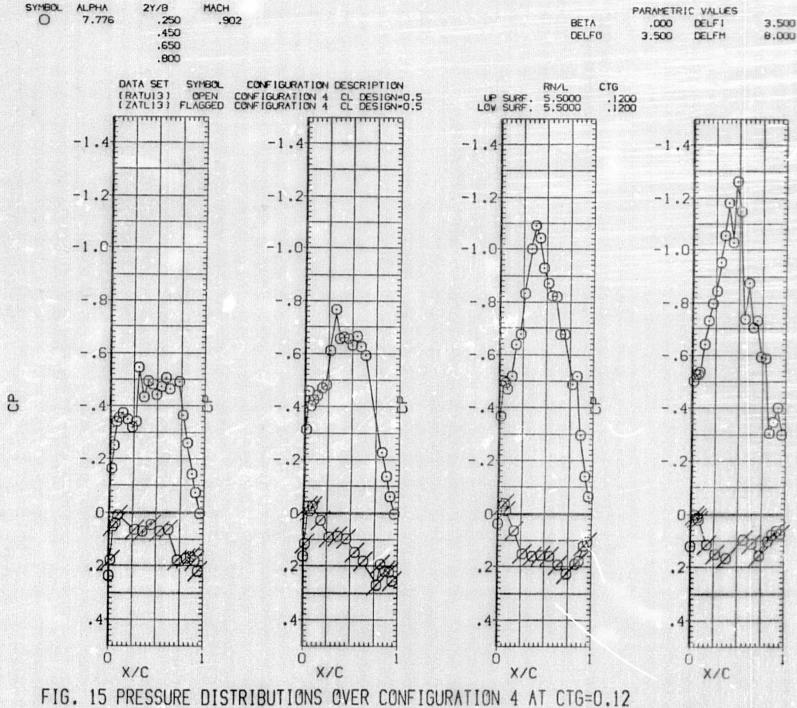


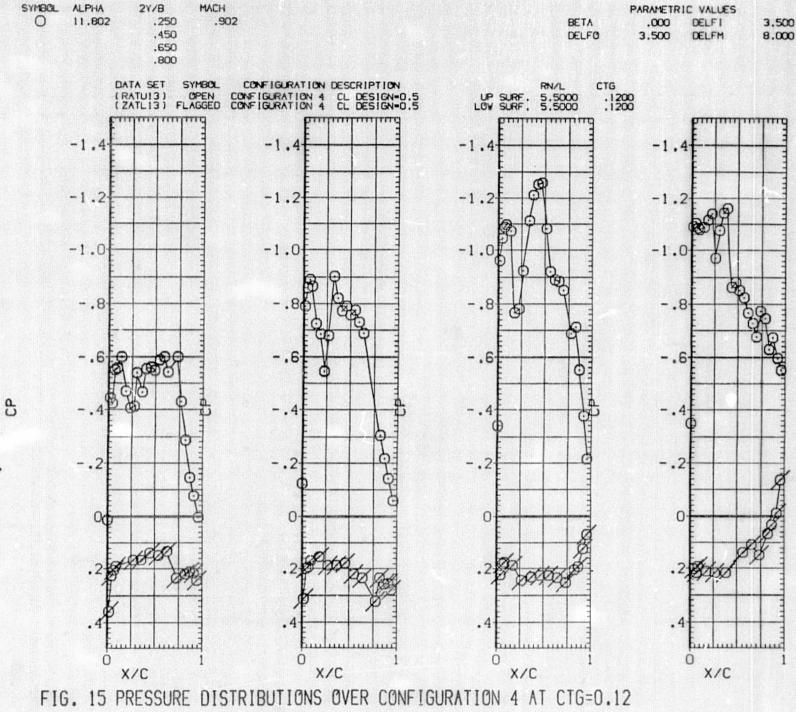
FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 4 AT CTG=0.0







MACH



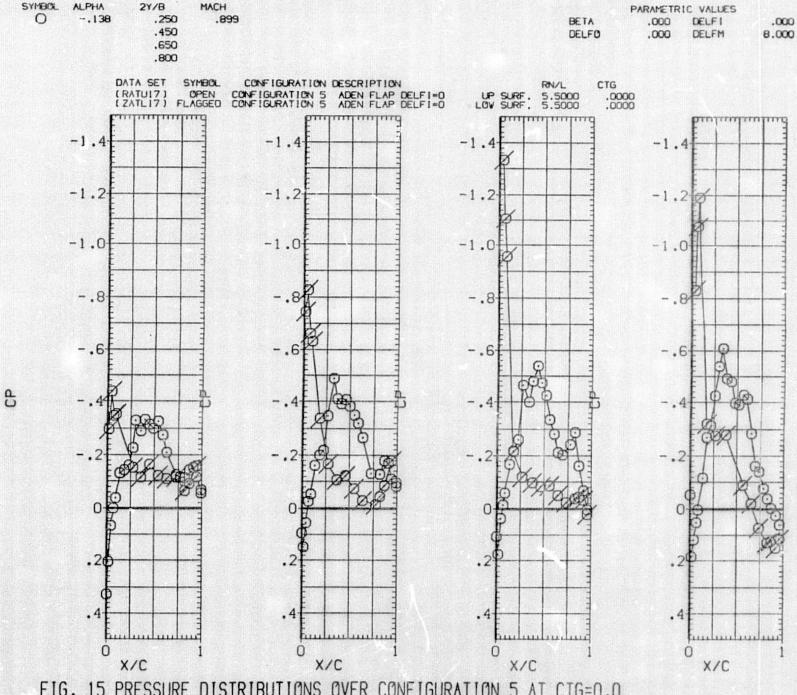
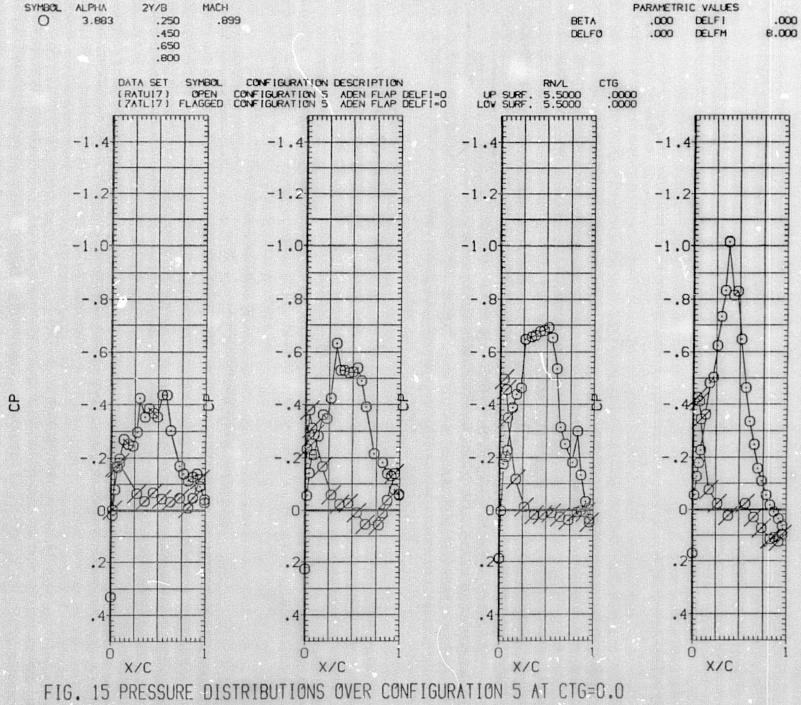


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.0



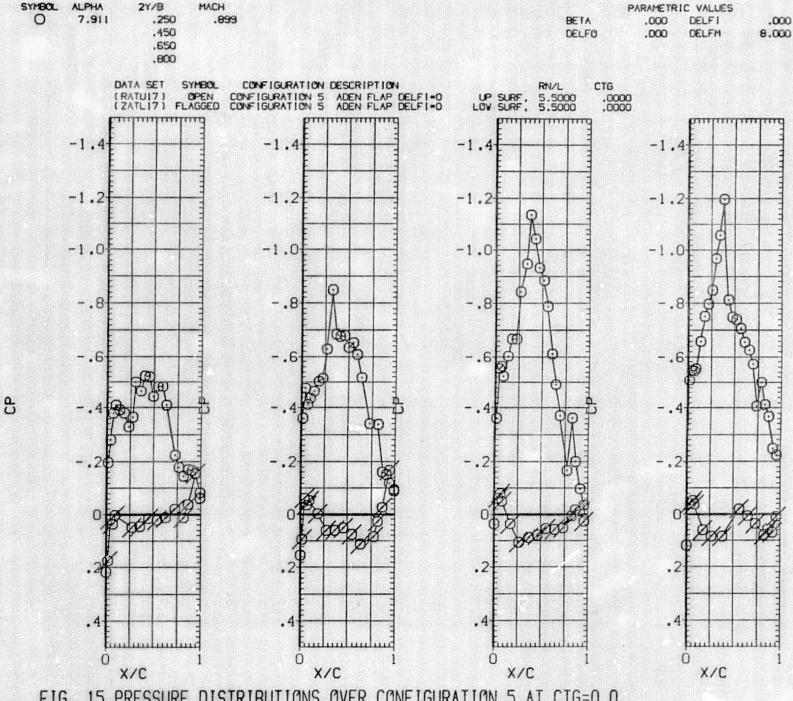
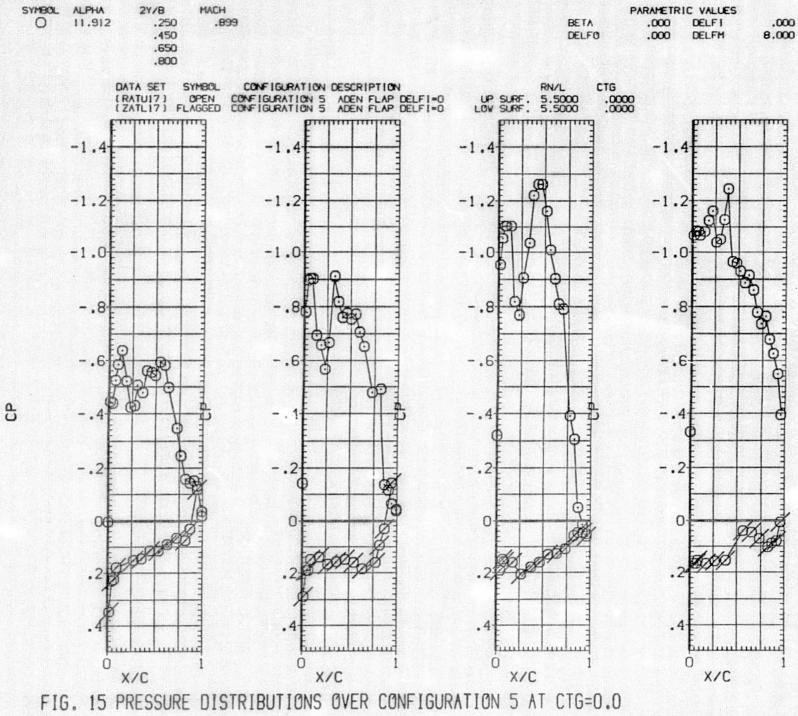


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.0



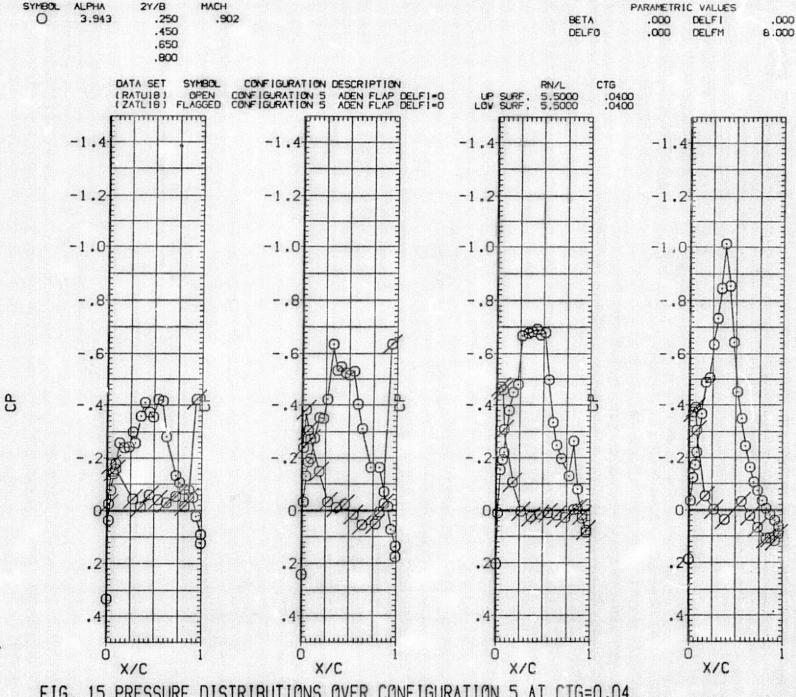


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.04

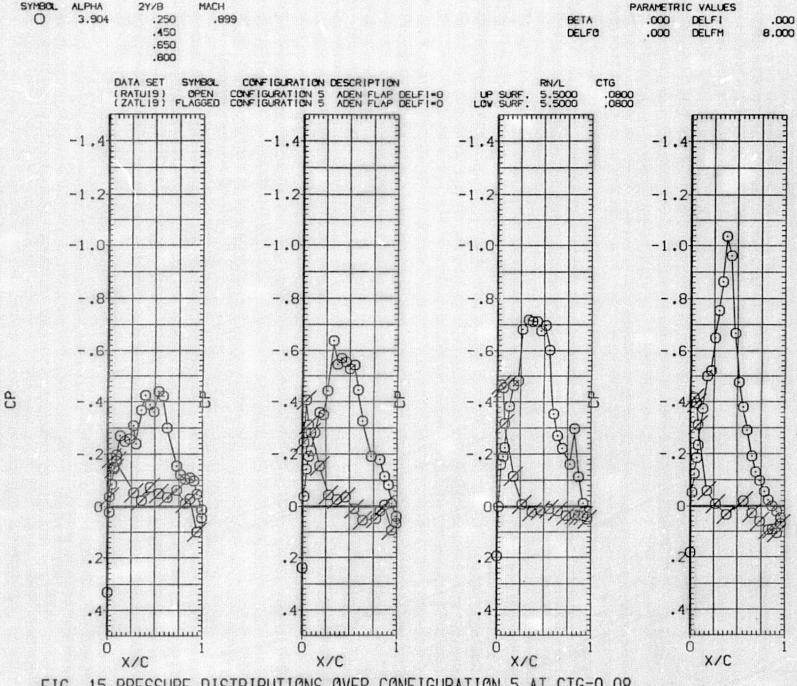


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.08

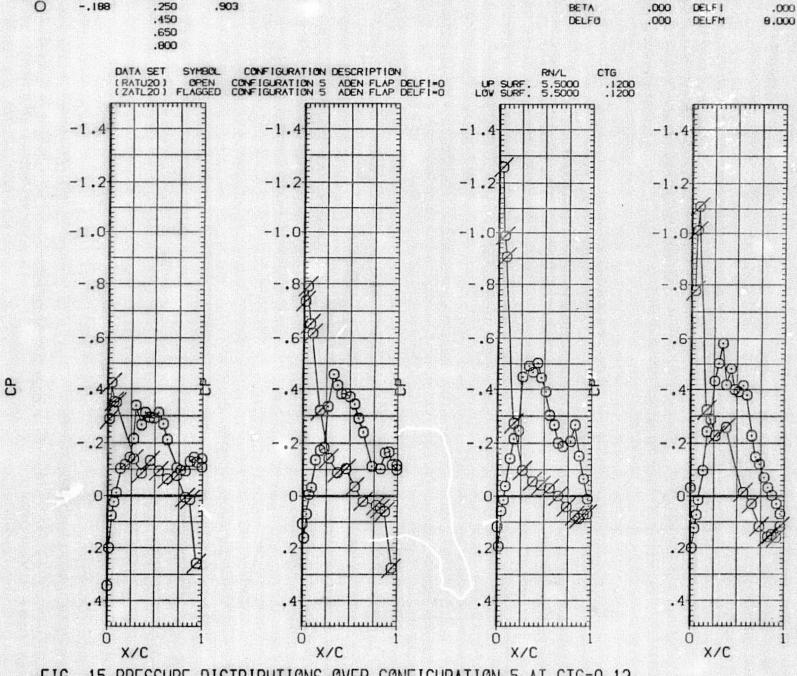


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.12

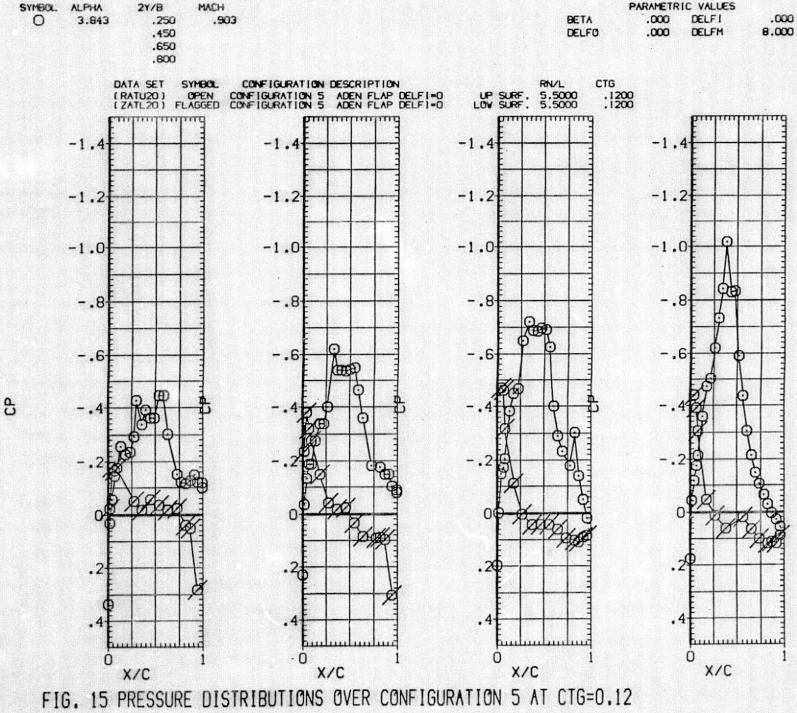
MACH

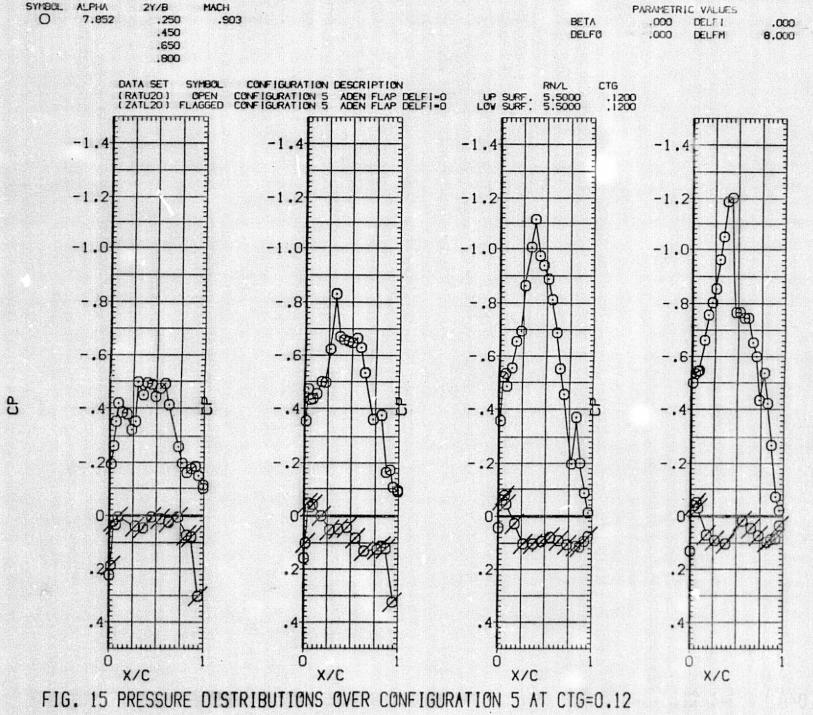
2Y/B

SYMBOL

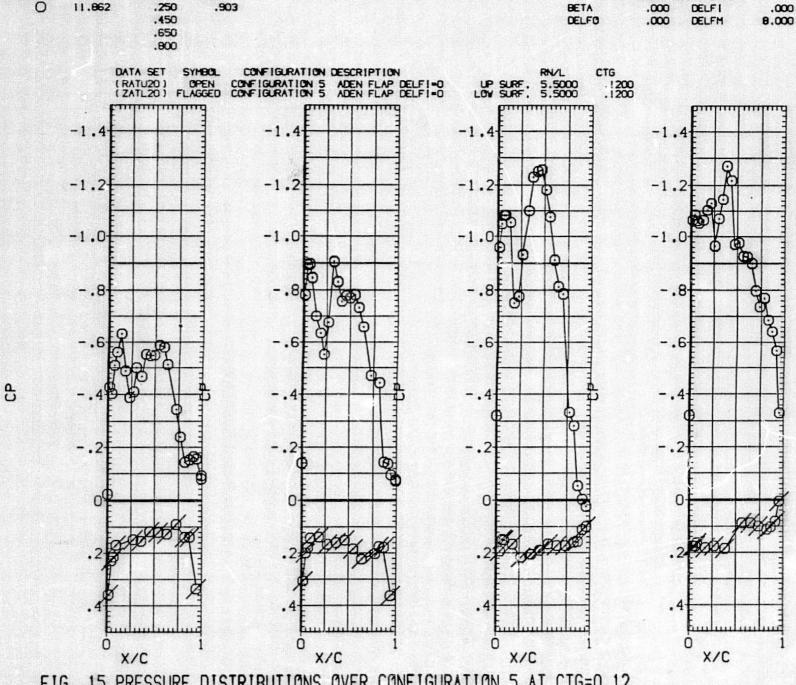
ALPHA

PARAMETRIC VALUES





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MACH

2Y/B

SYMBOL

ALPHA

FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 5 AT CTG=0.12

PARAMETRIC VALUES

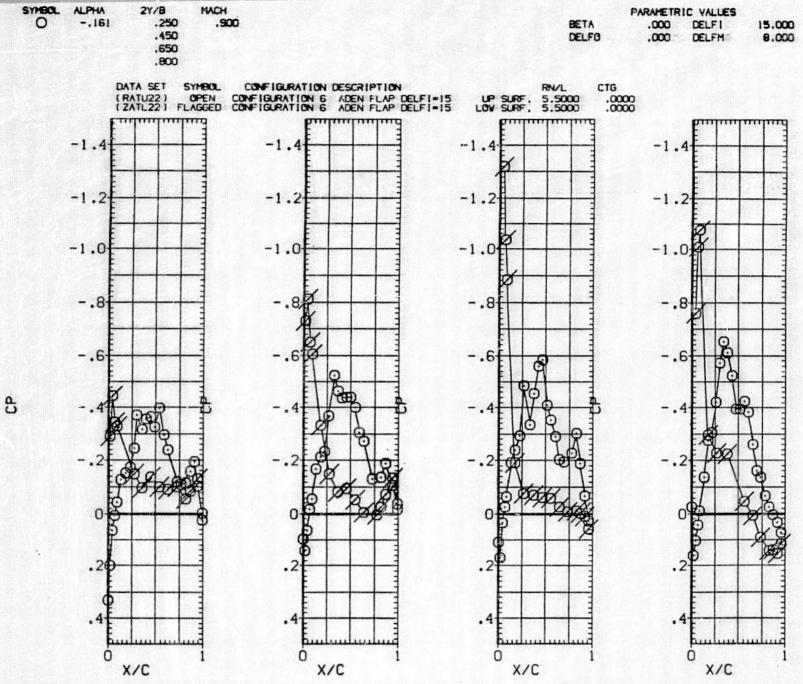
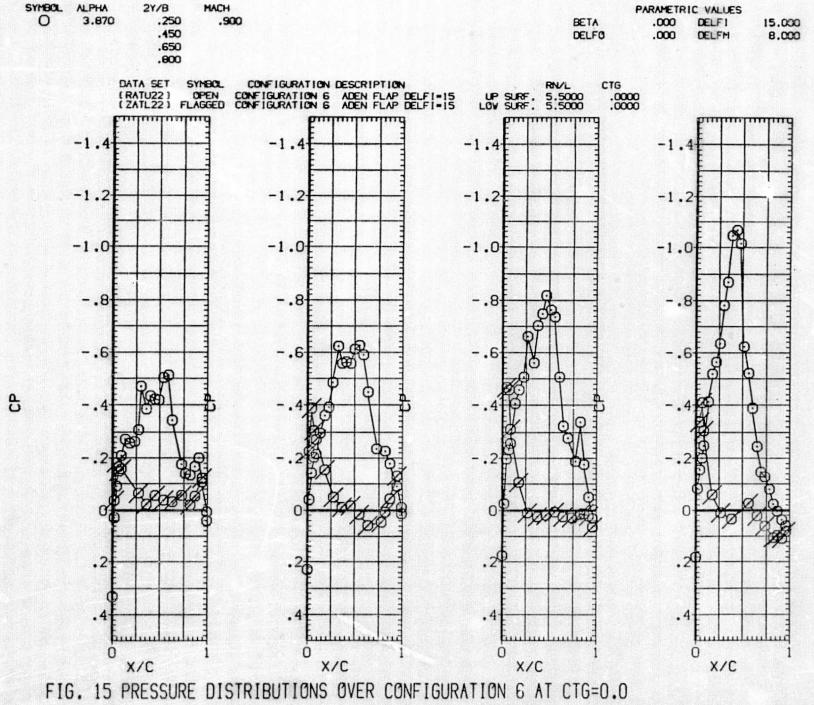


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.0



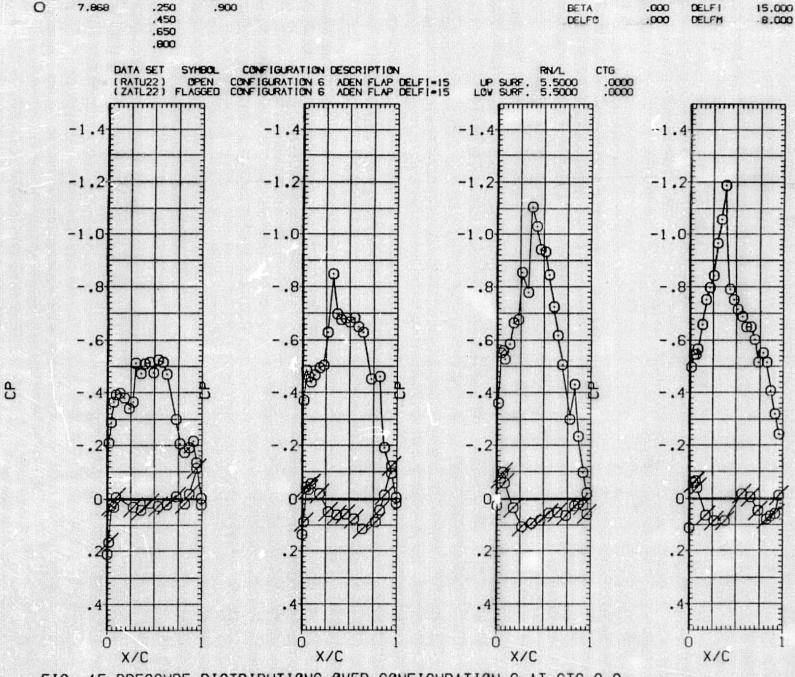


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.0

ALPHA

2Y/B

MACH

SYMBOL

PARAMETRIC VALUES

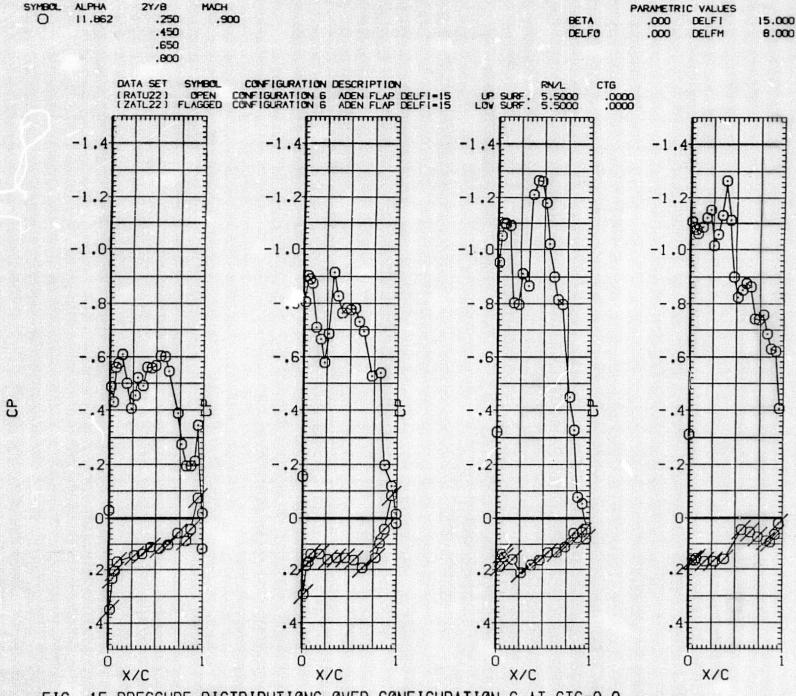
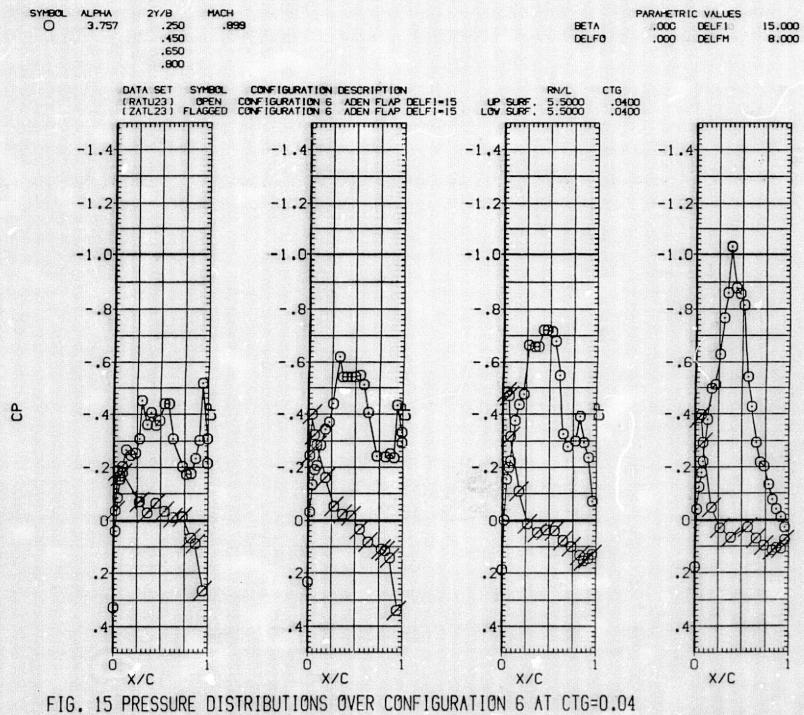


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.0



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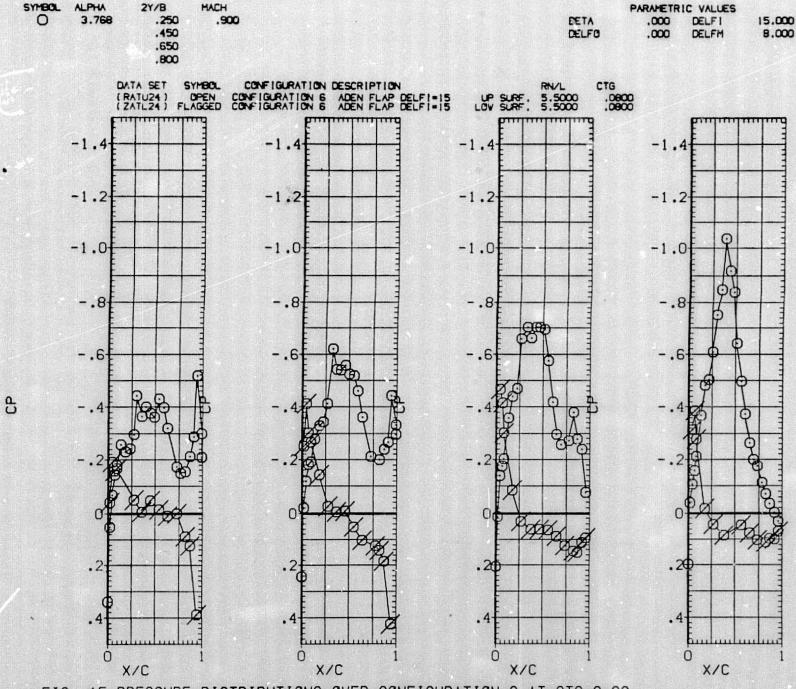


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.08

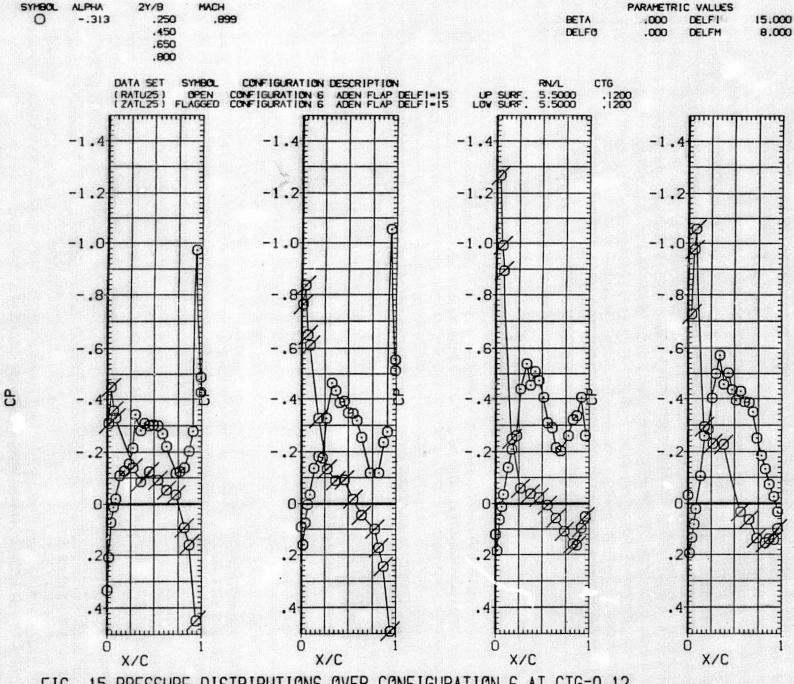


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.12

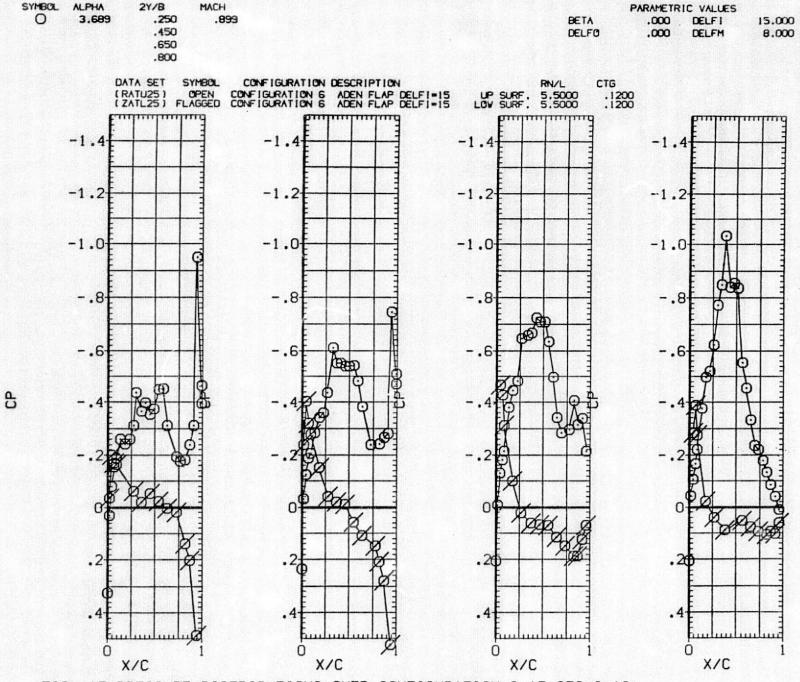


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.12

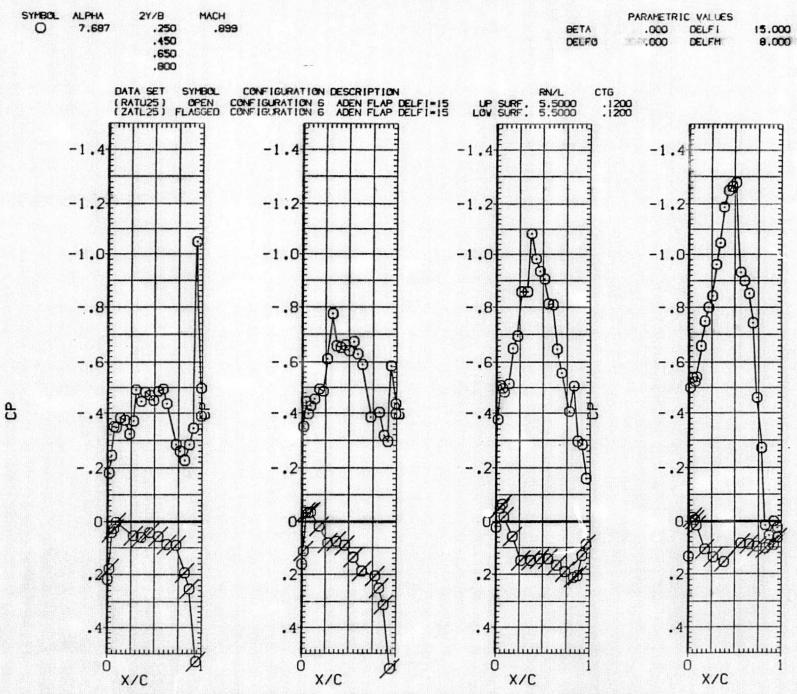


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.12

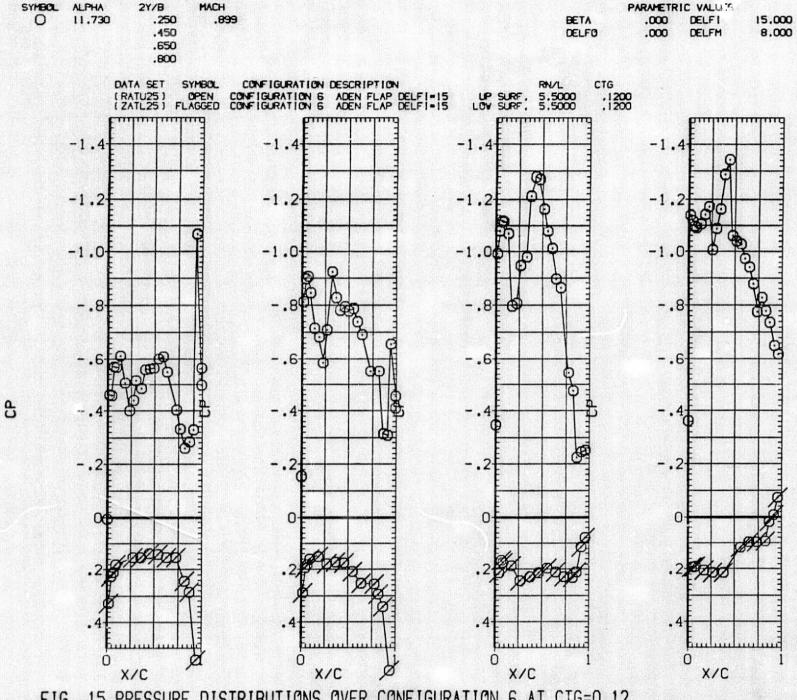


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 6 AT CTG=0.12

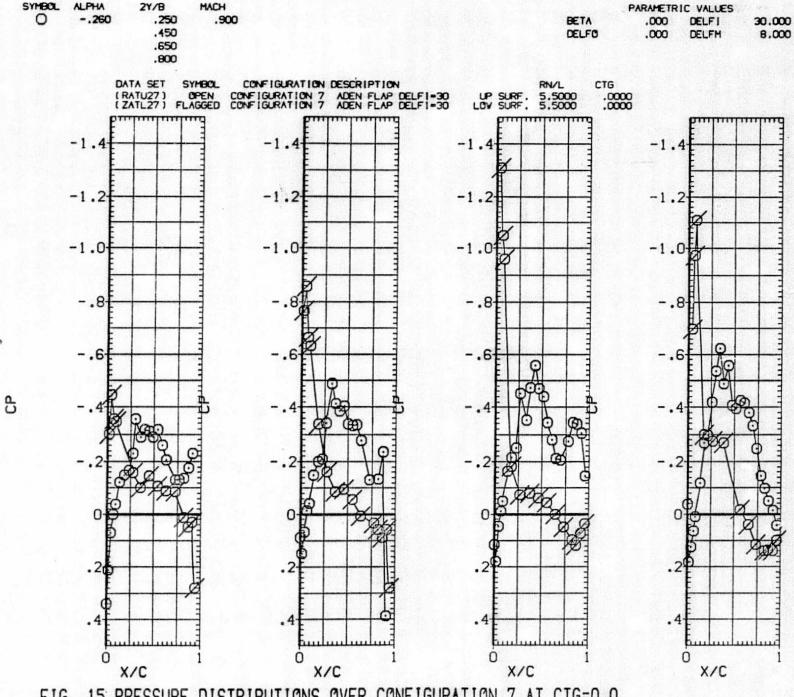
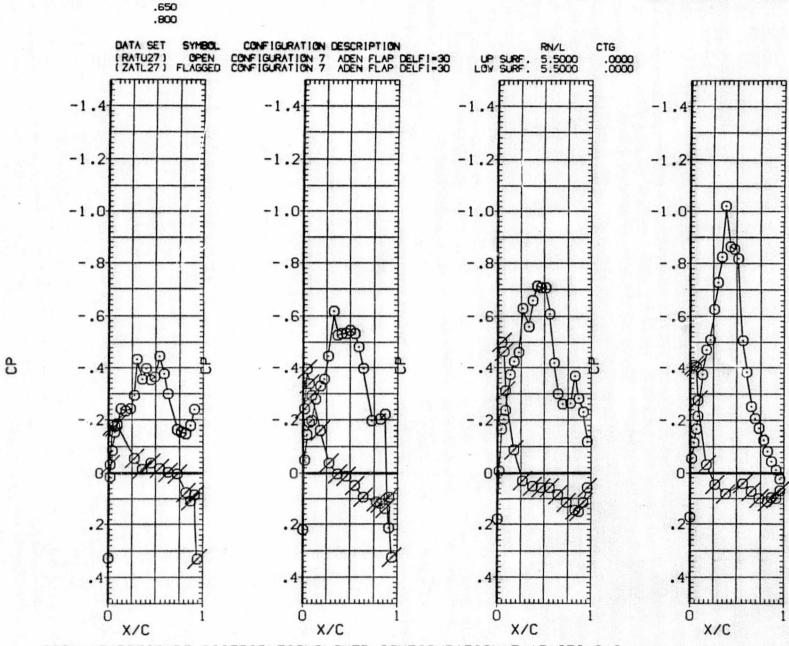


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 7 AT CTG=0.0



.450

FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 7 AT CTG=0.0

30,000

8,000

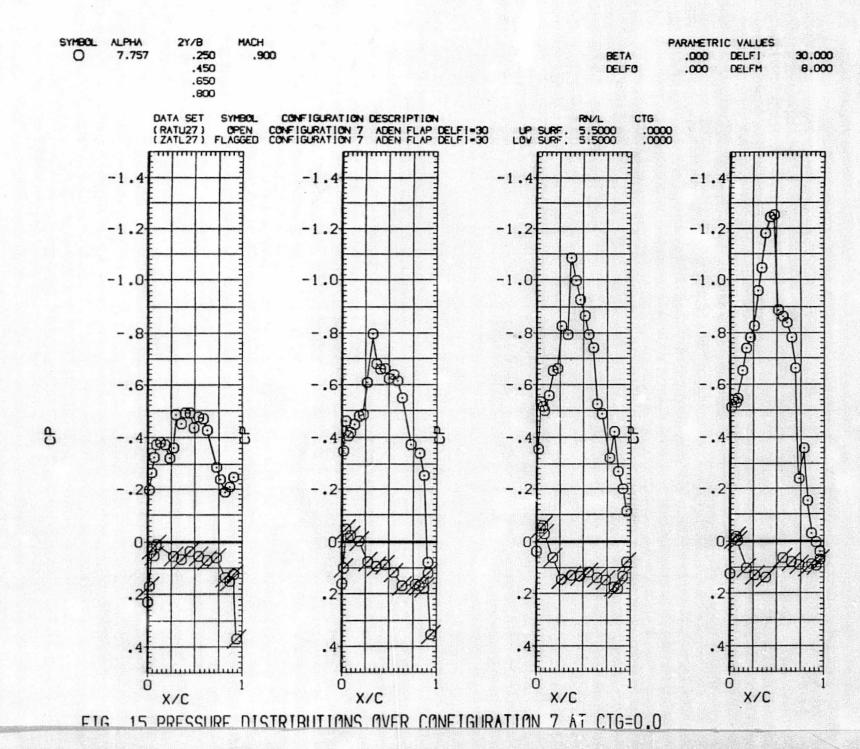
DELFI

DELFM

.000

BETA

ELFO



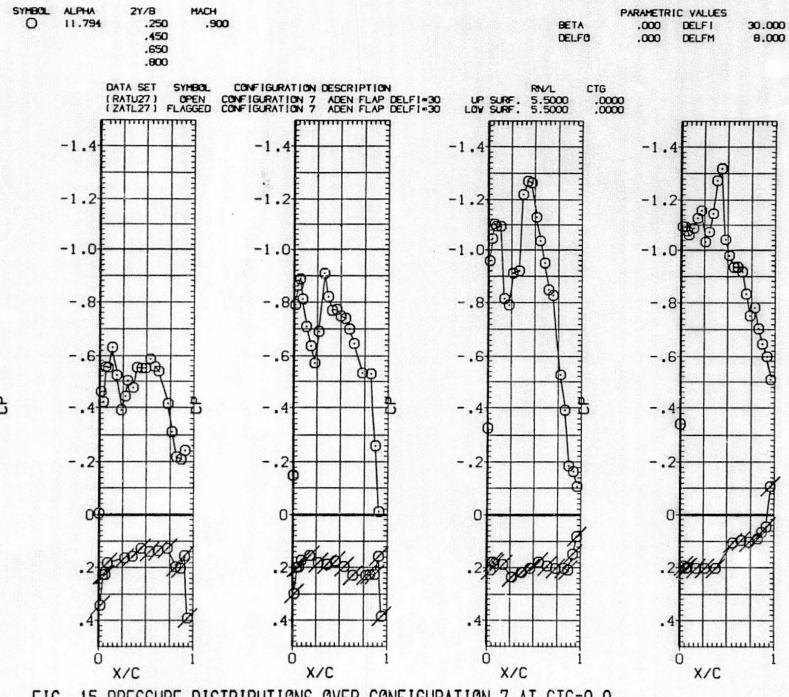


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 7 AT CTG=0.0

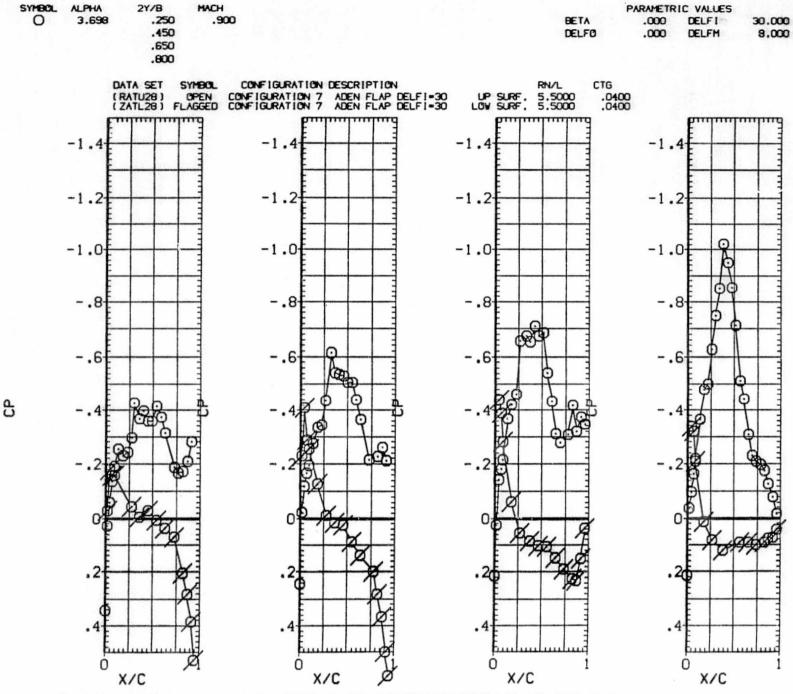
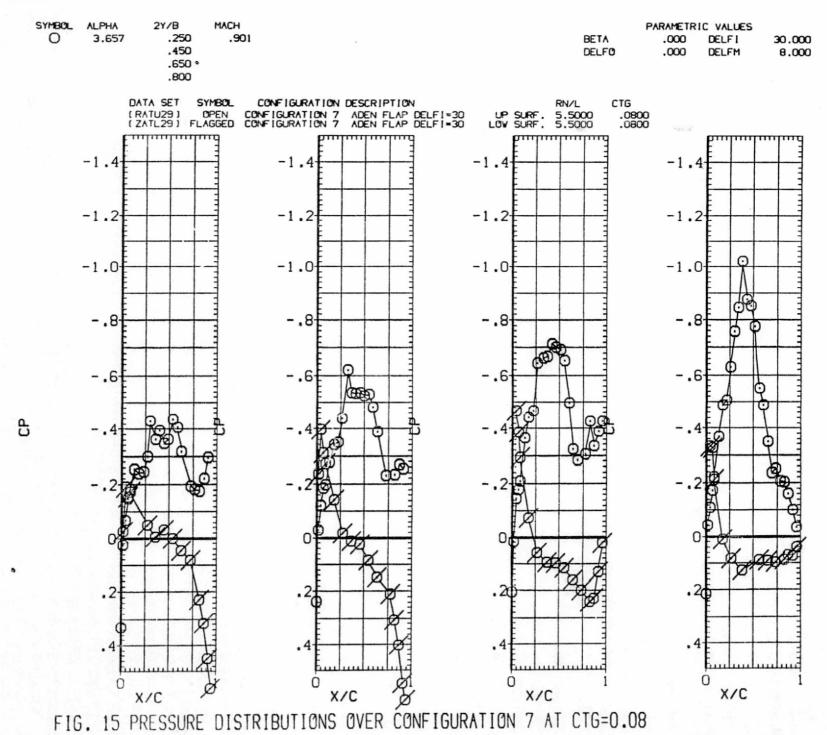


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 7 AT CTG=0.04



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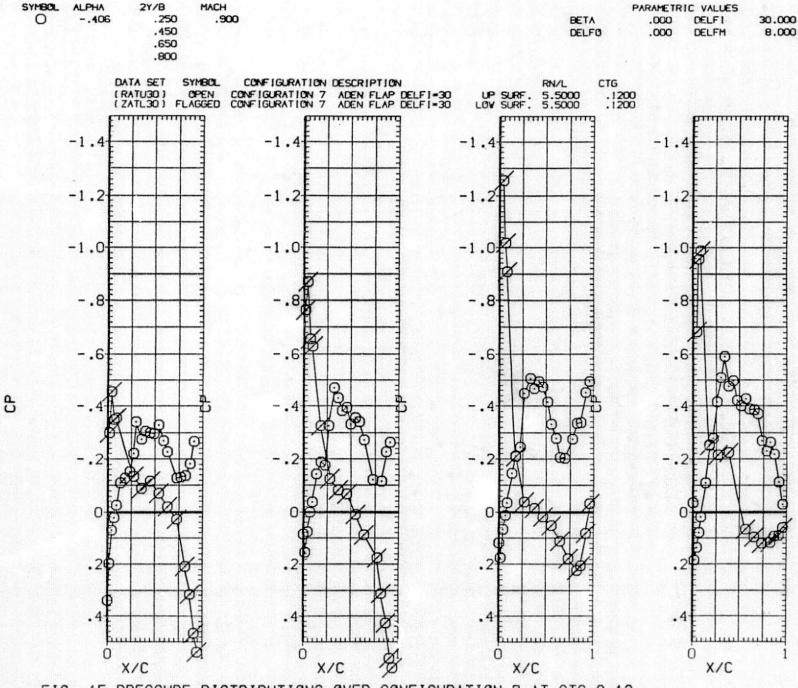


FIG. 15 PRESSURE DISTRIBUTIONS OVER CONFIGURATION 7 AT CTG=0.12

